

**UNIT 4**

**BIPOLAR JUNCTION TRANSISTORS**



## 4-1 ■ TRANSISTOR CONSTRUCTION

The basic structure of the bipolar junction transistor (BJT) determines its operating characteristics. In this section, you will see how semiconductor materials are used to form a transistor, and you will learn the standard transistor symbols.

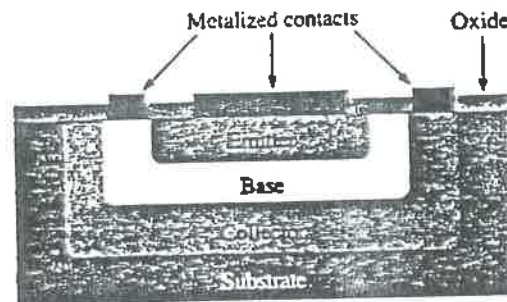
After completing this section, you should be able to

- Describe the basic structure of the bipolar junction transistor
  - Explain the difference between the structure of an *npn* and a *pnp* transistor
  - Identify the symbols for *npn* and *pnp* transistors
  - Name the three regions of a BJT and their labels

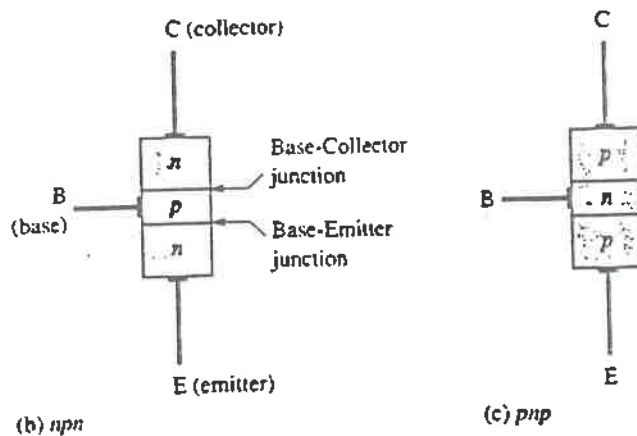
The bipolar junction transistor (BJT) is constructed with three doped semiconductor regions separated by two *pn* junctions, as shown in the epitaxial planar structure in Figure 4-1(a). The three regions are called emitter, base, and collector. Physical representations of the two types of bipolar transistors are shown in Figure 4-1(b) and (c). One type consists of two *n* regions separated by a *p* region (*npn*), and the other consists of two *p* regions separated by an *n* region (*pnp*).

The *pn* junction joining the base region and the emitter region is called the *base-emitter junction*. The junction joining the base region and the collector region is called the *base-collector junction*, as indicated in Figure 4-1(b). A wire lead connects to each of the three regions, as shown. These leads are labeled E, B, and C for emitter, base, and collector, respectively.

FIGURE 4-1  
Basic bipolar transistor construction.

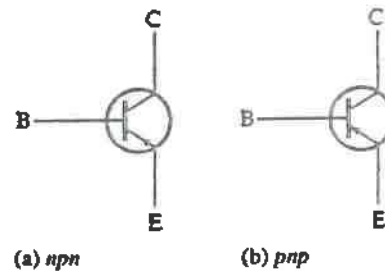


(a) Basic epitaxial planar structure



The base region is lightly doped and very thin compared to the heavily doped emitter and the moderately doped collector regions. (The reason for this is discussed in the next section.) Figure 4-2 shows the schematic symbols for the *npn* and *pnp* bipolar transistors. The term bipolar refers to the use of both holes and electrons as carriers in the transistor structure.

FIGURE 4-2  
Standard bipolar junction transistor (BJT)  
symbols.



## SECTION 4-1 REVIEW

1. Name the two types of BJTs according to their construction.
2. The BJT is a three-terminal device. Name the three terminals.
3. What separates the three regions in a BJT?

## 4-2 ■ BASIC TRANSISTOR OPERATION

*In order for the transistor to operate properly as an amplifier, the two pn junctions must be correctly biased with external dc voltages. In this section, we use the npn transistor for illustration. The operation of the pnp is the same as for the npn except that the roles of the electrons and holes, the bias voltage polarities, and the current directions are all reversed.*

*After completing this section, you should be able to*

- Explain how a transistor is biased and discuss the transistor currents and their relationships
  - Describe forward-reverse bias
  - Show how to connect a transistor to the bias-voltage sources
  - Describe the basic internal operation of a transistor
  - State the formula relating the collector, emitter, and base currents in a transistor

Figure 4-3 shows the proper bias arrangement for both *npn* and *pnp* transistors for active operation as an amplifier. Notice that in both cases the base-emitter (BE) junction is forward-biased and the base-collector (BC) junction is reverse-biased.

To illustrate transistor action let's examine what happens inside the *npn* transistor when the junctions are forward-reverse biased. The forward bias from base to emitter narrows the BE depletion region, and the reverse bias from base to collector widens the BC depletion region, as depicted in Figure 4-4. The heavily doped *n*-type emitter region is teeming with conduction-band (free) electrons that easily diffuse through the forward-

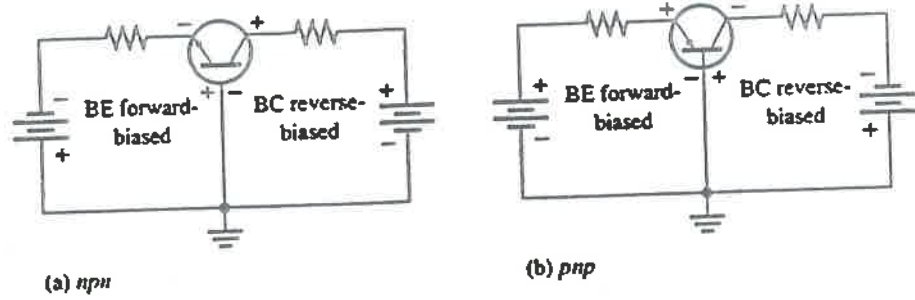


FIGURE 4-3  
Forward-reverse bias of a bipolar transistor.

biased BE junction into the *p*-type base region where they become minority carriers, just as in a forward-biased diode. The base region is lightly doped and very thin so that it has a very limited number of holes. Thus, only a small percentage of all the electrons flowing through the BE junction can combine with the available holes in the base. These relatively few recombined electrons flow out of the base lead as valence electrons, forming the small base electron current, as shown in Figure 4-4.

Most of the electrons flowing from the emitter into the thin, lightly doped base region do not recombine but diffuse into the BC depletion region. Once in this region they are pulled through the reverse-biased BC junction by the electric field set up by the force of attraction between the positive and negative ions. Actually, you can think of the electrons as being pulled across the reverse-biased BC junction by the attraction of the collector supply voltage. The electrons now move through the collector region, out

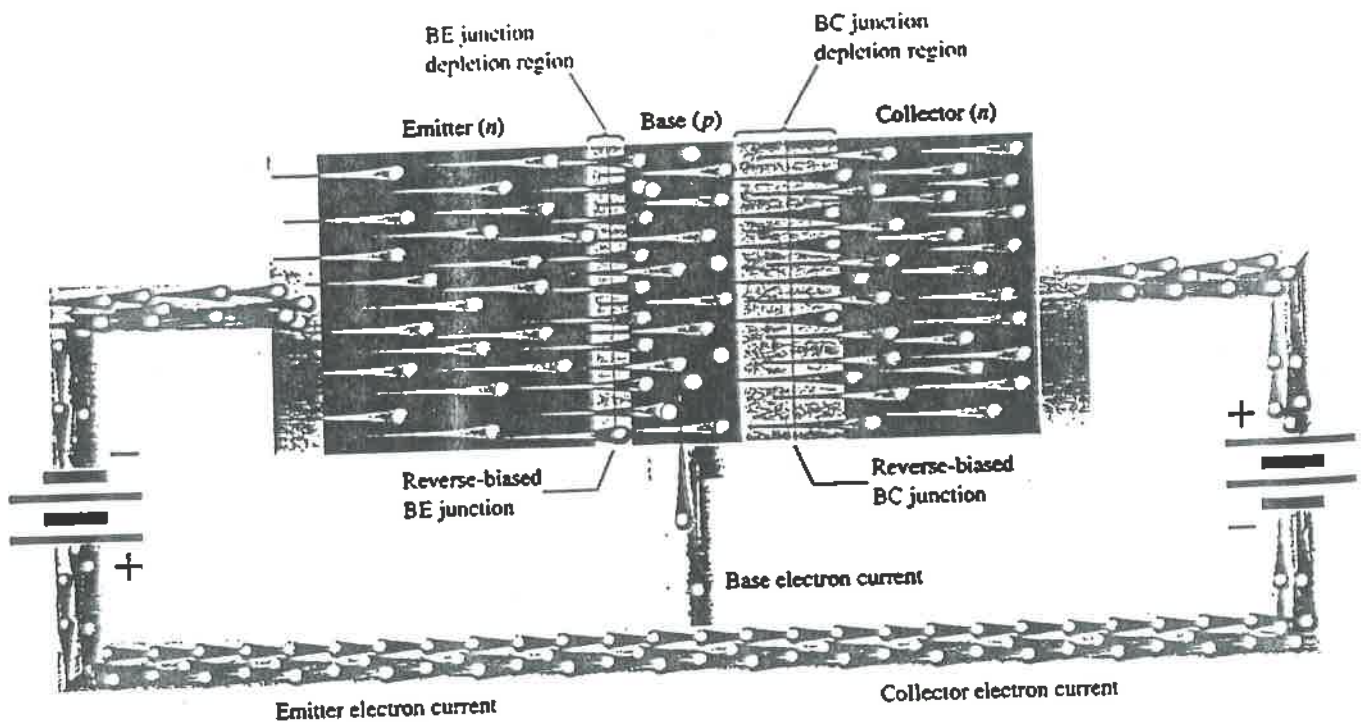


FIGURE 4-4  
Illustration of BJT action.

through the collector lead, and into the positive terminal of the collector voltage source. This forms the collector electron current, as shown in Figure 4-4.

### Transistor Currents

The directions of the currents in an *npn* transistor are as shown in Figure 4-5(a), and those for a *pnp* are shown in Figure 4-5(b). The currents are indicated on the corresponding schematic symbols in parts (c) and (d) of the figure. Notice that the arrow on the emitter of the transistor symbols points in the direction of conventional current. These diagrams show that the emitter current ( $I_E$ ) is the sum of the collector current ( $I_C$ ) and the base current ( $I_B$ ), expressed as follows:

$$I_E = I_C + I_B \quad (4-1)$$

As mentioned before,  $I_B$  is very small compared to  $I_E$  or  $I_C$ . The uppercase subscripts indicate dc values.

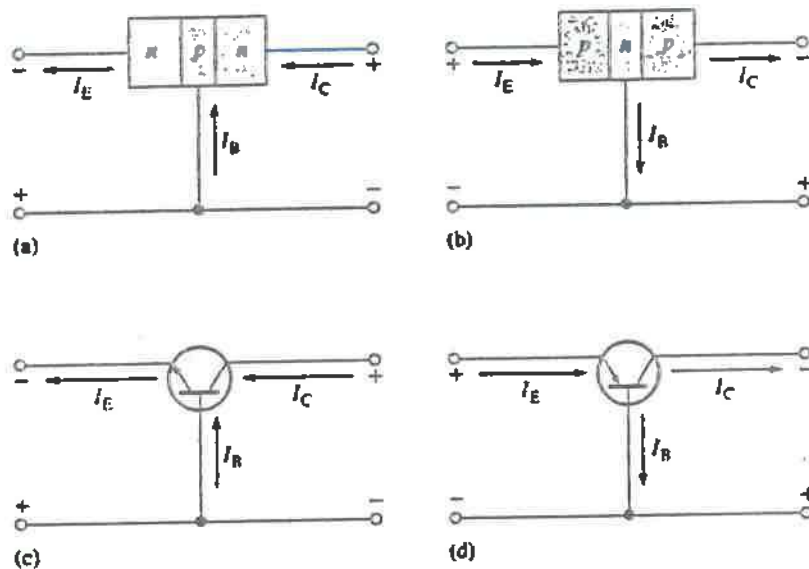


FIGURE 4-5  
Transistor currents.

### SECTION 4-2 REVIEW

1. What are the bias conditions of the base-emitter and base-collector junctions for a transistor to operate as an amplifier?
2. Which is the largest of the three transistor currents?
3. Is the base current smaller or larger than the emitter current?
4. Is the base region much thinner or much wider than the collector and emitter regions?
5. If the collector current is 1 mA and the base current is 10  $\mu$ A, what is the emitter current?

## 4-3 ■ TRANSISTOR CHARACTERISTICS AND PARAMETERS

In this section, you will first learn how to set up a dc circuit to properly bias a transistor. Two important parameters,  $\beta_{DC}$  (dc current gain) and  $\alpha_{DC}$  are introduced and used to analyze a transistor circuit. Also, transistor characteristic curves are covered, and you will learn how a transistor's operation can be determined from these curves. Finally, maximum ratings of a transistor are discussed.

After completing this section, you should be able to

- Discuss transistor parameters and characteristics and use these to analyze a transistor circuit
  - Define dc beta ( $\beta_{DC}$ )
  - Define dc alpha ( $\alpha_{DC}$ )
  - State the mathematical relationship between  $\beta_{DC}$  and  $\alpha_{DC}$
  - Identify all currents and voltages in a transistor circuit
  - Analyze a basic transistor dc circuit
  - Interpret collector characteristic curves and use a dc load line
  - Describe how  $\beta_{DC}$  varies with temperature and collector current
  - Discuss and apply maximum transistor ratings
  - Derate a transistor for power dissipation
  - Interpret a transistor data sheet

When a transistor is connected to bias voltages, as shown in Figure 4-6 for both *npn* and *pnp* types,  $V_{BB}$  forward-biases the base-emitter junction, and  $V_{CC}$  reverse-biases the base-collector junction. Although in this chapter we are using battery symbols to represent the bias voltages, in practice the voltages are usually derived from a dc power supply. For example,  $V_{CC}$  is usually taken directly from the power supply output and  $V_{BB}$  (which is smaller) can be produced with a voltage divider. Bias arrangements are examined thoroughly in Chapter 5.

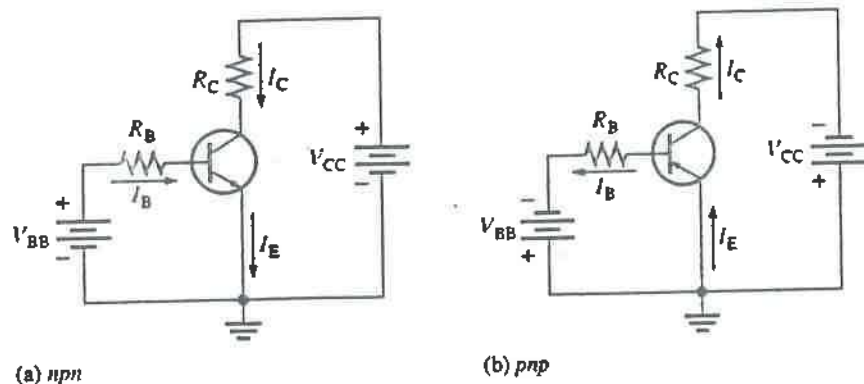


FIGURE 4-6  
Transistor dc bias circuits.

**DC Beta ( $\beta_{DC}$ ) and DC Alpha ( $\alpha_{DC}$ )**

The ratio of the collector current  $I_C$  to the base current  $I_B$  is the dc beta ( $\beta_{DC}$ ), which is the dc current gain of a transistor.

$$\beta_{DC} = \frac{I_C}{I_B} \quad (4-2)$$

Typical values of  $\beta_{DC}$  range from less than 20 to 200 or higher.  $\beta_{DC}$  is usually designated as  $h_{FE}$  on transistor data sheets.

$$h_{FE} = \beta_{DC}$$

The ratio of the collector current  $I_C$  to the emitter current  $I_E$  is the dc alpha ( $\alpha_{DC}$ ).

$$\alpha_{DC} = \frac{I_C}{I_E} \quad (4-3)$$

Typically, values of  $\alpha_{DC}$  range from 0.95 to 0.99 or greater, but  $\alpha_{DC}$  is always less than 1. The reason is that  $I_C$  is always slightly less than  $I_E$  by the amount of  $I_B$ . For example, if  $I_E = 100$  mA and  $I_B = 1$  mA, then  $I_C = 99$  mA and  $\alpha_{DC} = 0.99$ .

**Relationship of  $\beta_{DC}$  and  $\alpha_{DC}$** 

Let's start with the current formula  $I_E = I_C + I_B$  and divide each current by  $I_C$ :

$$\frac{I_E}{I_C} = \frac{I_C}{I_C} + \frac{I_B}{I_C} = 1 + \frac{I_B}{I_C}$$

Since  $\beta_{DC} = I_C/I_B$  and  $\alpha_{DC} = I_C/I_E$ , we can substitute the reciprocals into the equation:

$$\frac{1}{\alpha_{DC}} = 1 + \frac{1}{\beta_{DC}}$$

By rearranging and solving for  $\beta_{DC}$ , we get

$$\begin{aligned} \frac{1}{\alpha_{DC}} &= \frac{\beta_{DC} + 1}{\beta_{DC}} \\ \beta_{DC} &= \alpha_{DC} (\beta_{DC} + 1) \\ \beta_{DC} &= \alpha_{DC} \beta_{DC} + \alpha_{DC} \\ \beta_{DC} - \alpha_{DC} \beta_{DC} &= \alpha_{DC} \\ \beta_{DC} (1 - \alpha_{DC}) &= \alpha_{DC} \end{aligned}$$

$$\beta_{DC} = \frac{\alpha_{DC}}{1 - \alpha_{DC}} \quad (4-4)$$

Equation (4-4) shows that the closer  $\alpha_{DC}$  is to 1, the higher the value of  $\beta_{DC}$ .

**EXAMPLE 4-1**

Determine  $\beta_{DC}$ ,  $I_E$ , and  $\alpha_{DC}$  for a transistor where  $I_B = 50 \mu\text{A}$  and  $I_C = 3.65 \text{ mA}$ .

*Solution*

$$\beta_{DC} = \frac{I_C}{I_B} = \frac{3.65 \text{ mA}}{50 \mu\text{A}} = 73$$

$$I_E = I_C + I_B = 3.65 \text{ mA} + 50 \mu\text{A} = 3.70 \text{ mA}$$

$$\alpha_{DC} = \frac{I_C}{I_E} = \frac{3.65 \text{ mA}}{3.70 \text{ mA}} = 0.986$$

*Related Exercise* A certain transistor has a  $\beta_{DC}$  of 200. When the base current is  $50 \mu\text{A}$ , determine the collector current. What is  $\alpha_{DC}$ ?

### Current and Voltage Analysis

Consider the circuit configuration in Figure 4-7. Three transistor currents and three dc voltages can be identified.

$I_B$ : base current (dc)

$I_E$ : emitter current (dc)

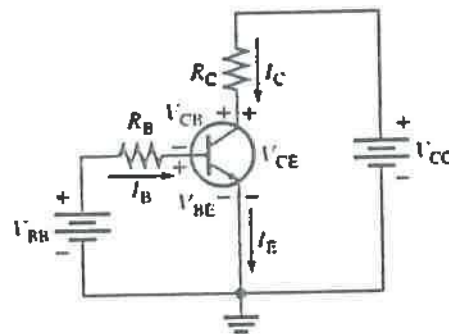
$I_C$ : collector current (dc)

$V_{BE}$ : dc voltage at base with respect to emitter

$V_{CB}$ : dc voltage at collector with respect to base

$V_{CE}$ : dc voltage at collector with respect to emitter

**FIGURE 4-7**  
Transistor currents and voltages.



$V_{BB}$  forward-biases the base-emitter junction and  $V_{CC}$  reverse-biases the base-collector junction. When the base-emitter junction is forward-biased, it is like a forward-biased diode and has a forward voltage drop of

$$V_{BE} \cong 0.7 \text{ V} \quad (4-5)$$

Since the emitter is at ground (0 V), by Kirchhoff's voltage law, the voltage across  $R_B$  is

$$V_{R_B} = V_{BB} - V_{BE}$$

Also, by Ohm's law,

$$V_{R_B} = I_B R_B$$

Substituting for  $V_{R_B}$  yields

$$I_B R_B = V_{BB} - V_{BE}$$

Solving for  $I_B$ , you get

$$I_B = \frac{V_{BB} - V_{BE}}{R_B} \quad (4-6)$$

The drop across  $R_C$  is

$$V_{R_C} = I_C R_C$$

The voltage at the collector with respect to the emitter, which is grounded, is

$$V_{CE} = V_{CC} - I_C R_C \quad (4-7)$$

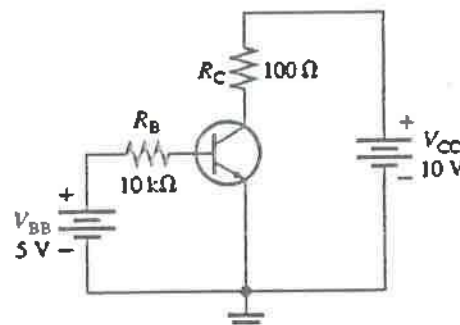
where  $I_C = \beta_{DC} I_B$ . The voltage across the reverse-biased collector-base junction is

$$V_{CB} = V_{CE} - V_{BE} \quad (4-8)$$

#### EXAMPLE 4-2

Determine  $I_B$ ,  $I_C$ ,  $I_E$ ,  $V_{BE}$ ,  $V_{CE}$ , and  $V_{CB}$  in the circuit of Figure 4-8. The transistor has a  $\beta_{DC} = 150$ .

FIGURE 4-8



**Solution** From Equation (4-5)  $V_{BE} = 0.7$  V. Calculate the base, collector, and emitter currents as follows:

$$I_B = \frac{V_{BB} - V_{BE}}{R_B} = \frac{5 \text{ V} - 0.7 \text{ V}}{10 \text{ k}\Omega} = 430 \mu\text{A}$$

$$I_C = \beta_{DC} I_B = (150)(430 \mu\text{A}) = 64.5 \text{ mA}$$

$$I_E = I_C + I_B = 64.5 \text{ mA} + 430 \mu\text{A} = 64.9 \text{ mA}$$

Solve for  $V_{CE}$  and  $V_{CB}$ :

$$\begin{aligned} V_{CE} &= V_{CC} - I_C R_C = 10 \text{ V} - (64.5 \text{ mA})(100 \Omega) \\ &= 10 \text{ V} - 6.45 \text{ V} = 3.55 \text{ V} \end{aligned}$$

$$V_{CB} = V_{CE} - V_{BE} = 3.55 \text{ V} - 0.7 \text{ V} = 2.85 \text{ V}$$

Since the collector is at a higher voltage than the base, the collector-base junction is reverse-biased.

**Related Exercise** Determine  $I_B$ ,  $I_C$ ,  $I_E$ ,  $V_{CE}$ , and  $V_{CB}$  in Figure 4-8 for the following values:  $R_B = 22 \text{ k}\Omega$ ,  $R_C = 220 \Omega$ ,  $V_{BB} = 6 \text{ V}$ ,  $V_{CC} = 9 \text{ V}$ , and  $\beta_{DC} = 90$ .

### Collector Characteristic Curves

Using a circuit like that shown in Figure 4-9(a), you can generate a set of collector characteristic curves that show how the collector current,  $I_C$ , varies with the collector-to-emitter voltage,  $V_{CE}$ , for specified values of base current,  $I_B$ . Notice in the circuit diagram that both  $V_{BB}$  and  $V_{CC}$  are variable sources of voltage.

Assume that  $V_{BB}$  is set to produce a certain value of  $I_B$  and  $V_{CC}$  is zero. For this condition, both the base-emitter junction and the base-collector junction are forward-biased because the base is at approximately 0.7 V while the emitter and the collector are at 0 V. The base current is through the base-emitter junction because of the low impedance path to ground and, therefore,  $I_C$  is zero. When both junctions are forward-biased, the transistor is in the saturation region of its operation.

As  $V_{CC}$  is increased,  $V_{CE}$  increases gradually as the collector current increases. This is indicated by the portion of the characteristic curve between points A and B in Figure 4-9(b).  $I_C$  increases as  $V_{CC}$  is increased because  $V_{CE}$  remains less than 0.7 V due to the forward-biased base-collector junction.

When  $V_{CE}$  exceeds 0.7 V, the base-collector junction becomes reverse-biased and the transistor goes into the *active* or *linear* region of its operation. Once the base-collector junction is reverse-biased,  $I_C$  levels off and remains essentially constant for a given value of  $I_B$  as  $V_{CE}$  continues to increase. Actually,  $I_C$  increases very slightly as  $V_{CE}$  increases due to widening of the base-collector depletion region. This results in fewer holes for recombination in the base region which effectively causes a slight increase in  $\beta_{DC}$ . This is shown by the portion of the characteristic curve between points B and C in Figure 4-9(b). For this portion of the characteristic curve, the value of  $I_C$  is determined only by the relationship expressed as  $I_C = \beta_{DC} I_B$ .

When  $V_{CE}$  reaches a sufficiently high voltage, the reverse-biased base-collector junction goes into breakdown; and the collector current increases rapidly as indicated by the part of the curve to the right of point C in Figure 4-9(b). A transistor should never be operated in this breakdown region.

A family of collector characteristic curves is produced when  $I_C$  versus  $V_{CE}$  is plotted for several values of  $I_B$ , as illustrated in Figure 4-9(c). When  $I_B = 0$ , the transistor is in the cutoff region although there is a very small collector leakage current as indicated. The amount of collector leakage current for  $I_B = 0$  is exaggerated on the graph for purposes of illustration.

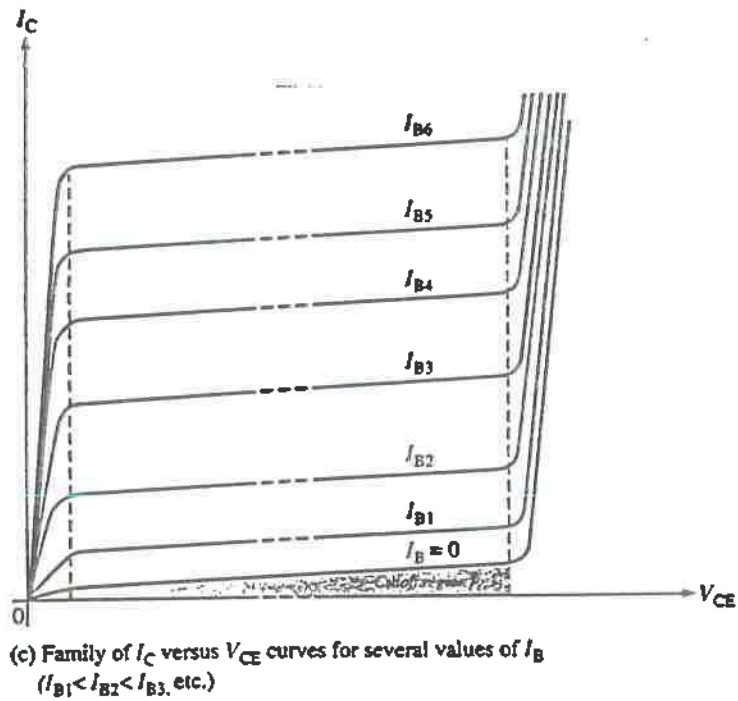
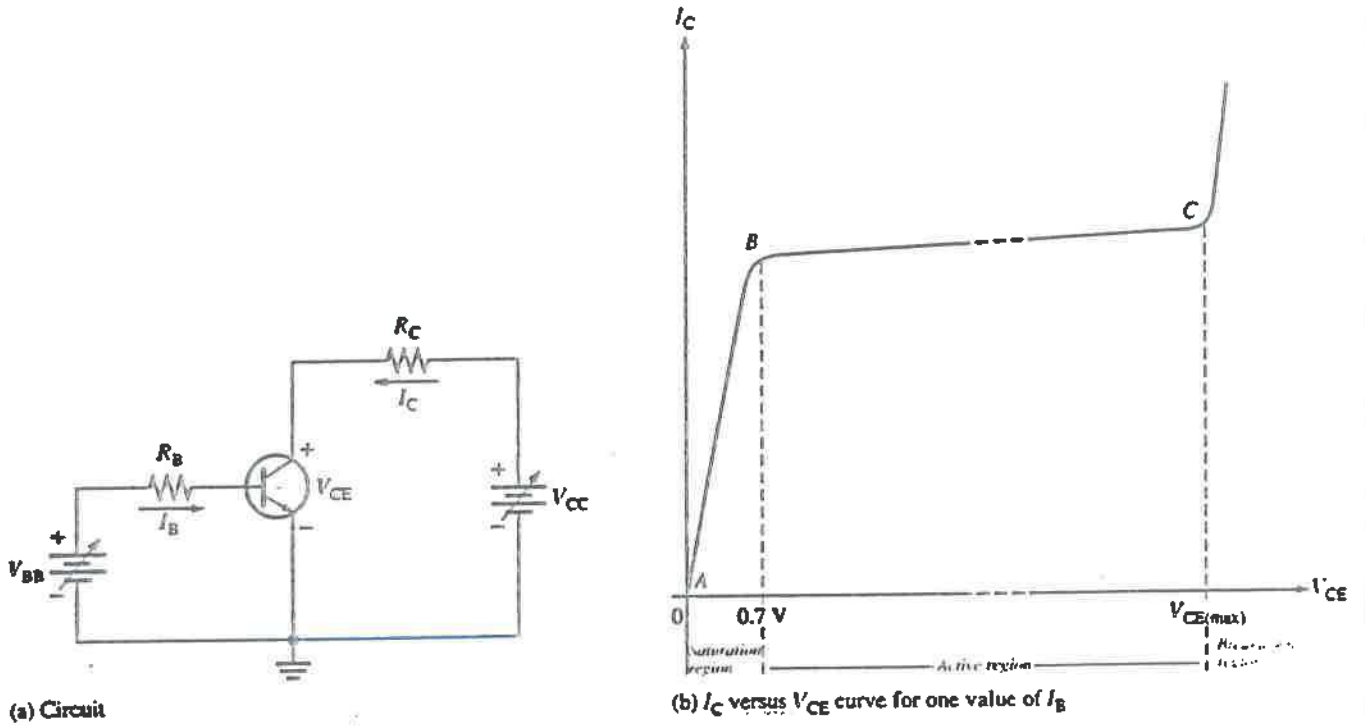
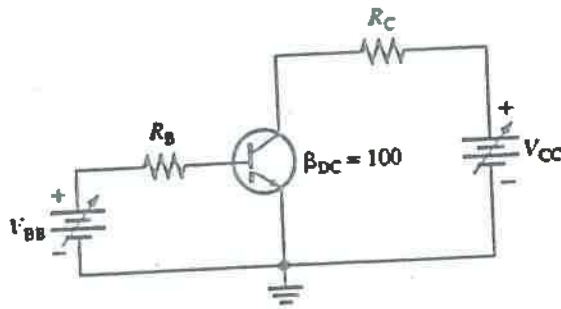


FIGURE 4-9  
Collector characteristic curves.

**EXAMPLE 4-3**

Sketch an ideal family of collector curves for the circuit in Figure 4-10 for  $I_B = 5 \mu\text{A}$  to  $25 \mu\text{A}$  in  $5 \mu\text{A}$  increments. Assume  $\beta_{DC} = 100$  and that  $V_{CE}$  does not exceed breakdown.

**FIGURE 4-10**

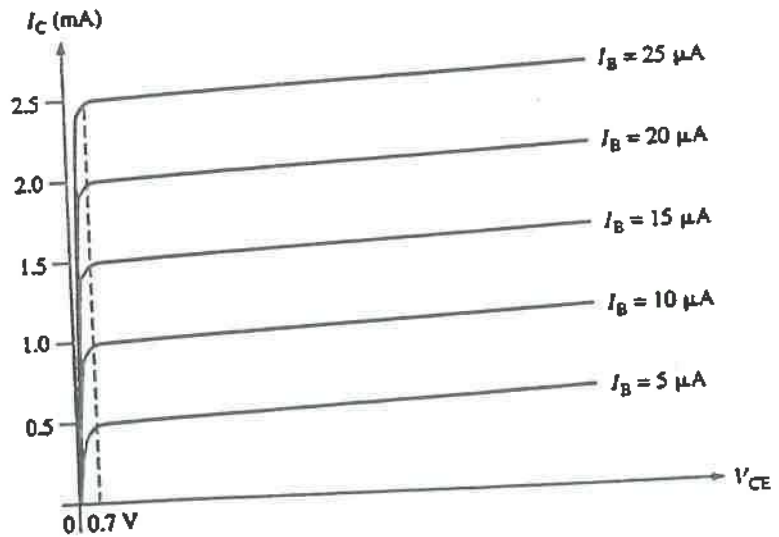


**Solution** Using the relationship  $I_C = \beta_{DC} I_B$ , values of  $I_C$  are calculated and tabulated in Table 4-1. The resulting curves are plotted in Figure 4-11. These are ideal curves because the slight increase in  $I_C$  for a given value of  $I_B$  as  $V_{CE}$  increases in the active region is neglected.

**TABLE 4-1**

$I_B$	$I_C$
$5 \mu\text{A}$	$0.5 \text{ mA}$
$10 \mu\text{A}$	$1.0 \text{ mA}$
$15 \mu\text{A}$	$1.5 \text{ mA}$
$20 \mu\text{A}$	$2.0 \text{ mA}$
$25 \mu\text{A}$	$2.5 \text{ mA}$

**FIGURE 4-11**

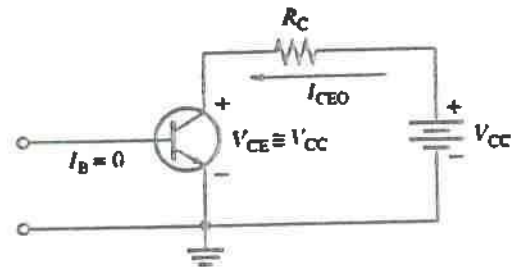


**Related Exercise** Where would the curve for  $I_B = 0$  appear on the graph in Figure 4-11, neglecting collector leakage current?

### Cutoff

As previously mentioned, when  $I_B = 0$ , the transistor is in the cutoff region of its operation. This is shown in Figure 4-12 with the base lead open, resulting in a base current of zero. Under this condition, there is a very small amount of collector leakage current,  $I_{CEO}$ , due mainly to thermally produced carriers. Because  $I_{CEO}$  is extremely small, it will usually be neglected in circuit analysis so that  $V_{CE} = V_{CC}$ . In cutoff, both the base-emitter and the base-collector junctions are reverse-biased.

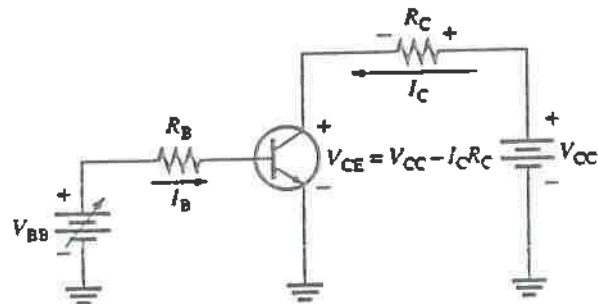
FIGURE 4-12  
Collector leakage current ( $I_{CEO}$ ) in cutoff.



### Saturation

When the base current in Figure 4-13(a) is increased, the collector current also increases ( $I_C = \beta_{DC} I_B$ ) and  $V_{CE}$  decreases as a result of more drop across the collector resistor ( $V_{CE} = V_{CC} - I_C R_C$ ). This is illustrated in Figure 4-13. When  $V_{CE}$  reaches its saturation value,  $V_{CE(sat)}$ , the base-collector junction becomes forward-biased and  $I_C$  can increase no further even with a continued increase in  $I_B$ . At the point of saturation, the relation  $I_C = \beta_{DC} I_B$  is no longer valid.  $V_{CE(sat)}$  for a transistor occurs somewhere below the knee of the collector curves, and it is usually only a few tenths of a volt for silicon transistors.

FIGURE 4-13  
As  $I_B$  increases due to increasing  $V_{BB}$ ,  $I_C$  also increases and  $V_{CE}$  decreases due to the increased voltage drop across  $R_C$ .



### DC Load Line

Cutoff and saturation can be illustrated in relation to the collector characteristic curves by the use of a load line. Figure 4-14 shows a dc load line drawn on a family of curves connecting the cutoff point and the saturation point. The bottom of the load line is at ideal cutoff where  $I_C = 0$  and  $V_{CE} = V_{CC}$ . The top of the load line is at saturation where  $I_C = I_{C(sat)}$  and  $V_{CE} = V_{CE(sat)}$ . In between cutoff and saturation along the load line is the active region of the transistor's operation. Load line operation is discussed more in a later chapter.

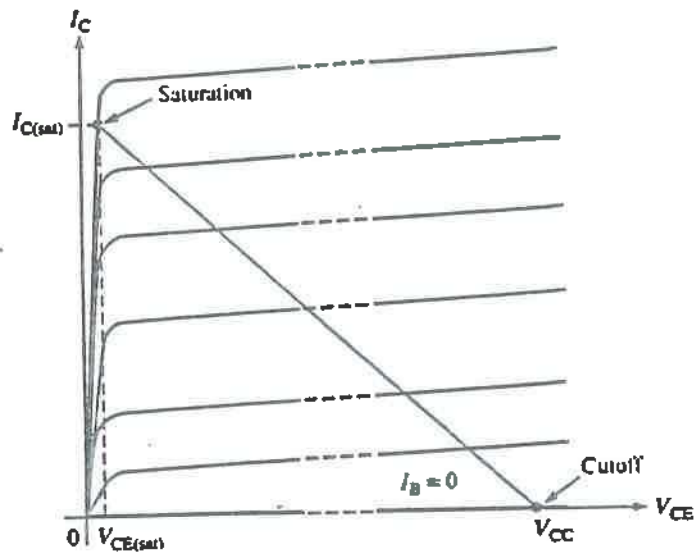
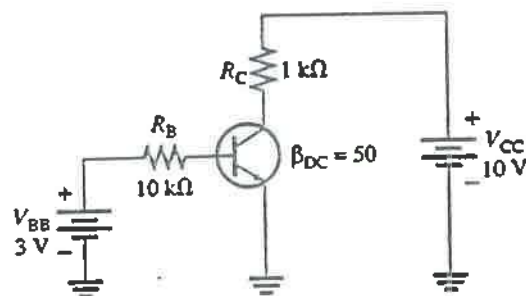


FIGURE 4-14  
DC load line on a family of collector characteristic curves illustrating the cutoff and saturation conditions.

#### EXAMPLE 4-4

Determine whether or not the transistor in Figure 4-15 is in saturation. Assume  $V_{CE(sat)} = 0.2 \text{ V}$ .

FIGURE 4-15



**Solution** First, determine  $I_{C(sat)}$ .

$$I_{C(sat)} = \frac{V_{CC} - V_{CE(sat)}}{R_C} = \frac{10 \text{ V} - 0.2 \text{ V}}{1 \text{ k}\Omega} = \frac{9.8 \text{ V}}{1 \text{ k}\Omega} = 9.8 \text{ mA}$$

Now, see if  $I_B$  is large enough to produce  $I_{C(sat)}$ .

$$I_B = \frac{V_{BB} - V_{BE}}{R_B} = \frac{3 \text{ V} - 0.7 \text{ V}}{10 \text{ k}\Omega} = \frac{2.3 \text{ V}}{10 \text{ k}\Omega} = 0.23 \text{ mA}$$

$$I_C = \beta_{DC} I_B = (50)(0.23 \text{ mA}) = 11.5 \text{ mA}$$

This shows that with the specified  $\beta_{DC}$ , this base current is capable of producing an  $I_C$  greater than  $I_{C(sat)}$ . Therefore, the transistor is saturated, and the collector current value

of 11.5 mA is never reached. If you further increase  $I_B$ , the collector current remains at its saturation value.

**Related Exercise** Determine whether or not the transistor in Figure 4-15 is saturated for the following values:  $\beta_{DC} = 125$ ,  $V_{BB} = 1.5$  V,  $R_B = 6.8$  k $\Omega$ ,  $R_C = 180$   $\Omega$ , and  $V_{CC} = 12$  V.

### More About $\beta_{DC}$

The  $\beta_{DC}$  or  $h_{FE}$  is a very important bipolar junction transistor parameter that we need to examine further.  $\beta_{DC}$  is not truly constant but varies with both collector current and with temperature. Keeping the junction temperature constant and increasing  $I_C$  causes  $\beta_{DC}$  to increase to a maximum. A further increase in  $I_C$  beyond this maximum point causes  $\beta_{DC}$  to decrease. If  $I_C$  is held constant and the temperature is varied,  $\beta_{DC}$  changes directly with the temperature. If the temperature goes up,  $\beta_{DC}$  goes up and vice versa. Figure 4-16 shows the variation of  $\beta_{DC}$  with  $I_C$  and junction temperature ( $T_J$ ) for a typical transistor.

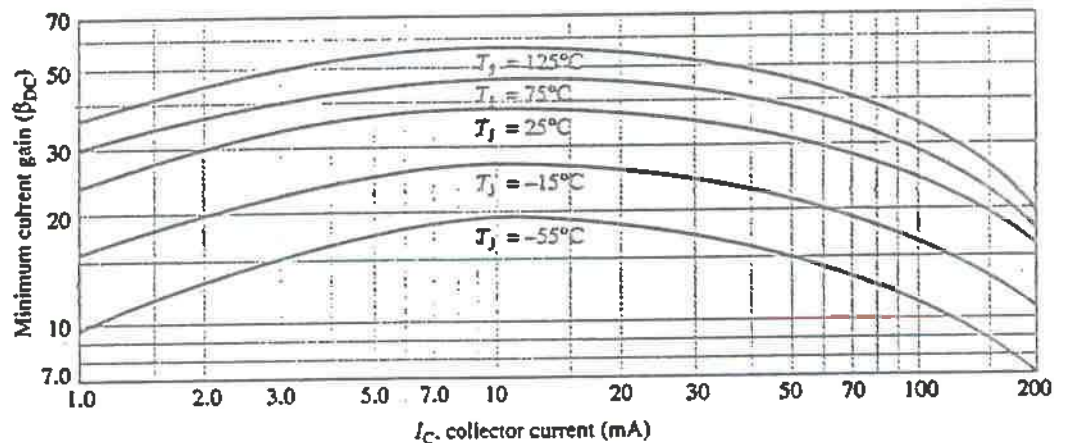


FIGURE 4-16  
Variation of  $\beta_{DC}$  with  $I_C$  for several temperatures.

A transistor data sheet usually specifies  $\beta_{DC}$  ( $h_{FE}$ ) at specific  $I_C$  values. Even at fixed values of  $I_C$  and temperature,  $\beta_{DC}$  varies from device to device for a given transistor due to inconsistencies in the manufacturing process that are unavoidable. The  $\beta_{DC}$  specified at a certain value of  $I_C$  is usually the minimum value,  $\beta_{DC(\min)}$ , although the maximum and typical values are also sometimes specified.

### Maximum Transistor Ratings

The transistor, like any other electronic device, has limitations on its operation. These limitations are stated in the form of maximum ratings and are normally specified on the manufacturer's data sheet. Typically, maximum ratings are given for collector-to-base voltage, collector-to-emitter voltage, emitter-to-base voltage, collector current, and power dissipation.

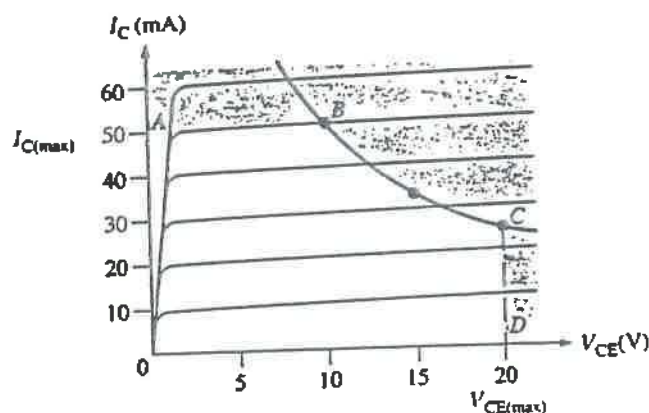
The product of  $V_{CE}$  and  $I_C$  must not exceed the maximum power dissipation. Both  $V_{CE}$  and  $I_C$  cannot be maximum at the same time. If  $V_{CE}$  is maximum,  $I_C$  can be calculated as

$$I_C = \frac{P_{D(max)}}{V_{CE}} \quad (4-9)$$

If  $I_C$  is maximum,  $V_{CE}$  can be calculated by rearranging Equation (4-9) as follows:

$$V_{CE} = \frac{P_{D(max)}}{I_C} \quad (4-10)$$

For any given transistor, a maximum power dissipation curve can be plotted on the collector characteristic curves, as shown in Figure 4-17(a). These values are tabulated in Figure 4-17(b). Assume  $P_{D(max)}$  is 500 mW,  $V_{CE(max)}$  is 20 V, and  $I_{C(max)}$  is 50 mA. The curve shows that this particular transistor cannot be operated in the shaded portion of the graph.  $I_{C(max)}$  is the limiting rating between points A and B,  $P_{D(max)}$  is the limiting rating between points B and C, and  $V_{CE(max)}$  is the limiting rating between points C and D.



$P_{D(max)}$	$V_{CE}$	$I_C$
500 mW	5 V	100 mA
500 mW	10 V	50 mA
500 mW	15 V	33 mA
500 mW	20 V	25 mA

(a)

(b)

FIGURE 4-17  
Maximum power dissipation curve.

#### EXAMPLE 4-5

A certain transistor is to be operated with  $V_{CE} = 6$  V. If its maximum power rating is 250 mW, what is the most collector current that it can handle?

**Solution**

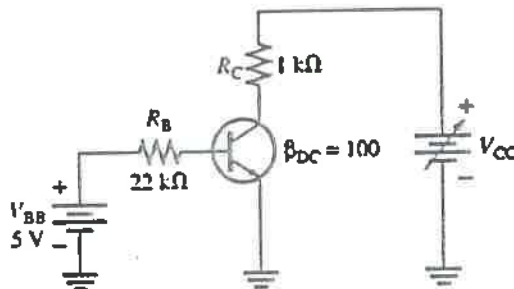
$$I_C = \frac{P_{D(max)}}{V_{CE}} = \frac{250 \text{ mW}}{6 \text{ V}} = 41.7 \text{ mA}$$

Remember that this is not necessarily the maximum  $I_C$ . The transistor can handle more collector current if  $V_{CE}$  is reduced, as long as  $P_{D(max)}$  is not exceeded.

**Related Exercise** If  $P_{D(max)} = 1$  W, how much voltage is allowed from collector to emitter if the transistor is operating with  $I_C = 100$  mA?

**EXAMPLE 4-6**

The transistor in Figure 4-18 has the following maximum ratings:  $P_{D(\max)} = 800 \text{ mW}$ ,  $V_{CE(\max)} = 15 \text{ V}$ , and  $I_{C(\max)} = 100 \text{ mA}$ . Determine the maximum value to which  $V_{CC}$  can be adjusted without exceeding a rating. Which rating would be exceeded first?

**FIGURE 4-18**

**Solution** First, find  $I_B$  so that you can determine  $I_C$ .

$$I_B = \frac{V_{BB} - V_{BE}}{R_B} = \frac{5 \text{ V} - 0.7 \text{ V}}{22 \text{ k}\Omega} = 195 \mu\text{A}$$

$$I_C = \beta_{DC} I_B = (100)(195 \mu\text{A}) = 19.5 \text{ mA}$$

$I_C$  is much less than  $I_{C(\max)}$  and will not change with  $V_{CC}$ . It is determined only by  $I_B$  and  $\beta_{DC}$ .

The voltage drop across  $R_C$  is

$$V_{RC} = I_C R_C = (19.5 \text{ mA})(1 \text{ k}\Omega) = 19.5 \text{ V}$$

Now you can determine the value of  $V_{CC}$  when  $V_{CE} = V_{CE(\max)} = 15 \text{ V}$ .

$$V_{RC} = V_{CC} - V_{CE}$$

So,

$$V_{CC(\max)} = V_{CE(\max)} + V_{RC} = 15 \text{ V} + 19.5 \text{ V} = 34.5 \text{ V}$$

$V_{CC}$  can be increased to 34.5 V, under the existing conditions, before  $V_{CE(\max)}$  is exceeded. However, at this point it is not known whether or not  $P_{D(\max)}$  has been exceeded.

$$P_D = V_{CE(\max)} I_C = (15 \text{ V})(19.5 \text{ mA}) = 293 \text{ mW}$$

Since  $P_{D(\max)}$  is 800 mW, it is *not* exceeded when  $V_{CC} = 34.5 \text{ V}$ . So,  $V_{CE(\max)} = 15 \text{ V}$  is the limiting rating in this case. If the base current is removed causing the transistor to turn off,  $V_{CE(\max)}$  will be exceeded because the entire supply voltage,  $V_{CC}$ , will be dropped across the transistor.

**Related Exercise** The transistor in Figure 4-18 has the following maximum ratings:  $P_{D(\max)} = 500 \text{ mW}$ ,  $V_{CE(\max)} = 25 \text{ V}$ , and  $I_{C(\max)} = 200 \text{ mA}$ . Determine the maximum value to which  $V_{CC}$  can be adjusted without exceeding a rating. Which rating would be exceeded first?

**Derating  $P_{D(max)}$** 

$P_{D(max)}$  is usually specified at 25°C. For higher temperatures,  $P_{D(max)}$  is less. Data sheets often give derating factors for determining  $P_{D(max)}$  at any temperature above 25°C. For example, a derating factor of 2 mW/C° indicates that the maximum power dissipation is reduced 2 mW for each Centigrade degree increase in temperature.

**EXAMPLE 4-7**

A certain transistor has a  $P_{D(max)}$  of 1 W at 25°C. The derating factor is 5 mW/C°. What is the  $P_{D(max)}$  at a temperature of 70°C?

**Solution** The change (reduction) in  $P_{D(max)}$  is

$$\Delta P_{D(max)} = (5 \text{ mW/C}^\circ)(70^\circ\text{C} - 25^\circ\text{C}) = (5 \text{ mW/C}^\circ)(45 \text{ C}^\circ) = 225 \text{ mW}$$

Therefore, the  $P_{D(max)}$  at 70°C is

$$1 \text{ W} - 225 \text{ mW} = 775 \text{ mW}$$

**Related Exercise** A transistor has a  $P_{D(max)} = 5 \text{ W}$  at 25°C. The derating factor is 10 mW/C°. What is the  $P_{D(max)}$  at 70°C?

**Transistor Data Sheet**

A partial data sheet for the 2N3903 and 2N3904 *npn* transistors is shown in Figure 4-19. Notice that the maximum collector-emitter voltage ( $V_{CEO}$ ) is 40 V. The "O" in the subscript indicates that the voltage is measured from collector (C) to emitter (E) with the base open (O). In the text, we use  $V_{CE(max)}$  for purposes of clarity. Also notice that the maximum collector current is 200 mA.

The  $\beta_{DC}$  ( $h_{FE}$ ) is specified for several values of  $I_C$  and, as you can see,  $h_{FE}$  varies with  $I_C$  as we previously discussed.

The collector-emitter saturation voltage,  $V_{CE(sat)}$  is 0.2 V maximum for  $I_{C(sat)} = 10 \text{ mA}$  and increases with the current.

**SECTION 4-3  
REVIEW**

1. Define  $\beta_{DC}$  and  $\alpha_{DC}$ . What is  $h_{FE}$ ?
2. If the dc current gain of a transistor is 100, determine  $\beta_{DC}$  and  $\alpha_{DC}$ .
3. What two variables are plotted on a collector characteristic curve?
4. What bias conditions must exist for a transistor to operate as an amplifier?
5. Does  $\beta_{DC}$  increase or decrease with temperature?
6. For a given type of transistor, can  $\beta_{DC}$  be considered to be a constant?

Maximum Ratings

Rating	Symbol	Value	Unit
Collector-Emitter voltage	$V_{CEO}$	40	V dc
Collector-Base voltage	$V_{CBO}$	60	V dc
Emitter-Base voltage	$V_{EBO}$	6.0	V dc
Collector current — continuous	$I_C$	200	mA dc
Total device dissipation @ $T_A = 25^\circ\text{C}$ Derate above $25^\circ\text{C}$	$P_D$	625 5.0	mW mW/°C
Total device dissipation @ $T_C = 25^\circ\text{C}$ Derate above $25^\circ\text{C}$	$P_D$	1.5 12	Watts mW/°C
Operating and storage junction Temperature range	$T_J, T_{stg}$	-55 to +150	°C

Thermal Characteristics

Characteristic	Symbol	Max	Unit
Thermal resistance, junction to case	$R_{\theta JC}$	83.3	°C/W
Thermal resistance, junction to ambient	$R_{\theta JA}$	200	°C/W

**2N3903**  
**2N3904**

General Purpose  
Transistors  
  
NPN Silicon

Electrical Characteristics ( $T_A = 25^\circ\text{C}$  unless otherwise noted.)

Characteristic	Symbol	Min	Max	Unit
<b>OFF Characteristics</b>				
Collector-Emitter breakdown voltage ( $I_C = 1.0$ mA dc, $I_B = 0$ )	$V_{(BR)CEO}$	40	—	V dc
Collector-Base breakdown voltage ( $I_C = 10$ $\mu$ A dc, $I_E = 0$ )	$V_{(BR)CBO}$	60	—	V dc
Emitter-Base breakdown voltage ( $I_E = 10$ $\mu$ A dc, $I_C = 0$ )	$V_{(BR)EBO}$	6.0	—	V dc
Base cutoff current ( $V_{CE} = 30$ V dc, $V_{EB} = 3.0$ V dc)	$I_{BL}$	—	50	nA dc
Collector cutoff current ( $V_{CE} = 30$ V dc, $V_{EB} = 3.0$ V dc)	$I_{CEX}$	—	50	nA dc
<b>ON Characteristics</b>				
DC current gain ( $I_C = 0.1$ mA dc, $V_{CE} = 1.0$ V dc)	$h_{FE}$	20	—	—
		40	—	
( $I_C = 1.0$ mA dc, $V_{CE} = 1.0$ V dc)	2N3903 2N3904	35	—	—
		70	—	
( $I_C = 10$ mA dc, $V_{CE} = 1.0$ V dc)	2N3903 2N3904	50	150	—
		100	300	
( $I_C = 50$ mA dc, $V_{CE} = 1.0$ V dc)	2N3903 2N3904	30	—	—
		60	—	
( $I_C = 100$ mA dc, $V_{CE} = 1.0$ V dc)	2N3903 2N3904	15	—	—
		30	—	
Collector-Emitter saturation voltage ( $I_C = 10$ mA dc, $I_B = 1.0$ mA dc) ( $I_C = 50$ mA dc, $I_B = 5.0$ mA dc)	$V_{CE(sat)}$	—	0.2 0.3	V dc
Base-Emitter saturation voltage ( $I_C = 10$ mA dc, $I_B = 1.0$ mA dc) ( $I_C = 50$ mA dc, $I_B = 5.0$ mA dc)	$V_{BE(sat)}$	0.65 —	0.85 0.95	V dc

FIGURE 4-19  
Partial transistor data sheet.

## 4-4 ■ THE TRANSISTOR AS AN AMPLIFIER

*Amplification is the process of linearly increasing the amplitude of an electrical signal and is one of the major properties of a transistor. As you learned, the transistor exhibits current gain (called  $\beta$ ). When a transistor is biased in the active (or linear) region, as previously described, the BE junction has a low resistance due to forward bias and the BC junction has a high resistance due to reverse bias.*

*After completing this section, you should be able to*

- Discuss how a transistor is used as a voltage amplifier
  - Describe amplification
  - Develop the ac equivalent circuit for a basic transistor amplifier
  - Determine the voltage gain of a basic transistor amplifier

## DC and AC Quantities

Before introducing the concept of transistor amplification, the designations that we will use for the circuit quantities of current, voltage, and resistance must be explained because amplifier circuits have both dc and ac quantities.

In this text, italic capital letters are used for both dc and ac currents ( $I$ ) and voltages ( $V$ ). This rule applies to rms, average, peak, and peak-to-peak ac values. AC current and voltage values are always rms unless stated otherwise. Although some texts use lowercase  $i$  and  $v$  for ac current and voltage, we reserve the use of lowercase  $i$  and  $v$  only for instantaneous values, as you learned in your dc/ac circuits course. In this text, the distinction between a dc current or voltage and an ac current or voltage is in the subscript.

DC quantities always carry an uppercase roman (nonitalic) subscript. For example,  $I_B$ ,  $I_C$ , and  $I_E$  are the dc transistor currents.  $V_{BE}$ ,  $V_{CB}$ , and  $V_{CE}$  are the dc voltages from one transistor terminal to another. Single subscripted voltages such as  $V_B$ ,  $V_C$ , and  $V_E$  are dc voltages from the transistor terminals to ground.

AC and all time-varying quantities always carry a lowercase italic subscript. For example,  $i_b$ ,  $i_c$ , and  $i_e$  are the ac transistor currents.  $v_{be}$ ,  $v_{cb}$ , and  $v_{ce}$  are the ac voltages from one transistor terminal to another. Single subscripted voltages such as  $v_b$ ,  $v_c$ , and  $v_e$  are ac voltages from the transistor terminals to ground.

The rule is different for *internal* transistor resistances. As you will see later, transistors have internal ac resistances that are designated by lowercase  $r'$  with an appropriate subscript. For example, the internal ac emitter resistance is designated as  $r'_e$ .

Circuit resistances external to the transistor itself use the standard italic capital  $R$  with a subscript that identifies the resistance as dc or ac (when applicable), just as for current and voltage. For example  $R_E$  is an external dc emitter resistance and  $R_e$  is an external ac emitter resistance.

## Transistor Amplification

As you have learned, a transistor amplifies current because the collector current is equal to the base current multiplied by the current gain,  $\beta$ . The base current in a transistor is very small compared to the collector and emitter currents. Because of this, the collector current is approximately equal to the emitter current.

With this in mind, let's look at the circuit in Figure 4-20(a). An ac voltage,  $V_{in}$  is superimposed on the dc bias voltage  $V_{BB}$  by connecting them in series with the base resistor,  $R_B$ , as shown. The dc bias voltage  $V_{CC}$  is connected to the collector through the collector resistor,  $R_C$ .

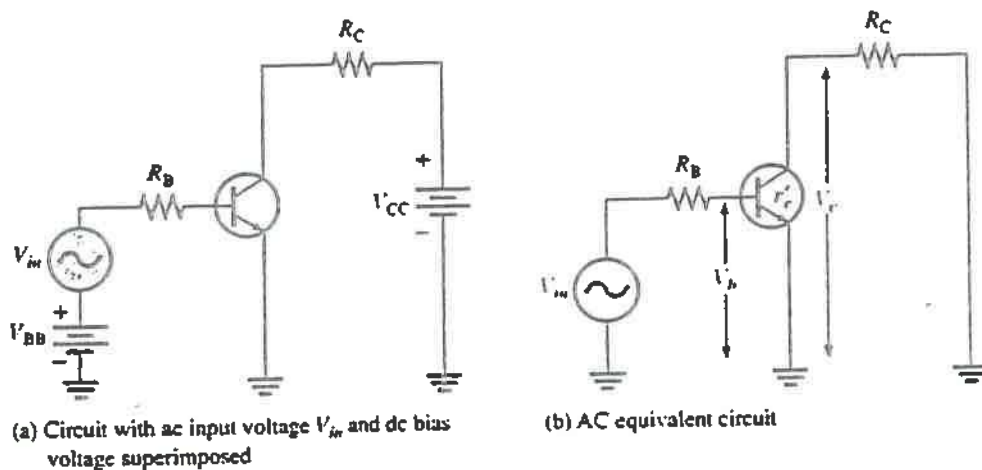


FIGURE 4-20  
Basic transistor amplifier circuit.

The ac input voltage produces an ac base current, which results in a much larger ac collector current. The ac collector current produces an ac voltage across  $R_C$ , thus producing an apparent amplified reproduction of the ac input voltage in the active region of operation.

**The AC Equivalent Circuit** The dc bias sources ideally appear as shorts to the ac voltage. Therefore, the ac equivalent circuit can be represented as shown in Figure 4-20(b) with  $V_{CC}$  and  $V_{BB}$  replaced by shorts.

The forward-biased base-emitter junction presents a very low resistance to the ac signal. This internal ac emitter resistance is designated  $r'_e$ . In Figure 4-20(b), the ac emitter current is

$$I_e \cong \frac{V_b}{r'_e}$$

The ac collector voltage,  $V_c$ , equals the ac voltage drop across  $R_C$ :

$$V_c = I_e R_C$$

Since  $I_c \cong I_e$ , the ac collector voltage is

$$V_c \cong I_e R_C$$

$V_b$  can be considered the transistor ac input voltage where  $V_b = V_{in} - I_b R_B$ .  $V_c$  can be considered the transistor ac output voltage. The ratio of  $V_c$  to  $V_b$  is the ac voltage gain,  $A_v$ , of the transistor circuit:

$$A_v = \frac{V_c}{V_b}$$

Substituting  $I_e R_C$  for  $V_c$  and  $I_e r'_e$  for  $V_b$ , we get

$$A_v = \frac{V_c}{V_b} \cong \frac{I_e R_C}{I_e r'_e}$$

The  $I_e$  terms cancel; therefore,

$$A_v \cong \frac{R_C}{r'_e} \quad (4-11)$$

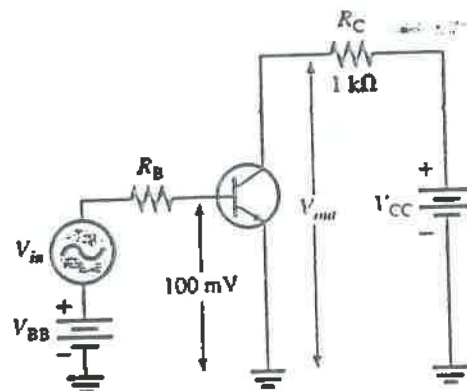
Equation (4-11) shows that the transistor in Figure 4-20 provides amplification or voltage gain dependent on the value of  $R_C$  and  $r'_e$ .

Since  $R_C$  is always considerably larger in value than  $r'_e$ , the output voltage is always greater than the input voltage. Various types of amplifiers are covered in detail in later chapters.

### EXAMPLE 4-8

Determine the voltage gain and the ac output voltage in Figure 4-21 if  $r'_e = 50 \Omega$ .

FIGURE 4-21



**Solution** The voltage gain is

$$A_v \cong \frac{R_C}{r'_e} = \frac{1 \text{ k}\Omega}{50 \Omega} = 20$$

Therefore, the ac output voltage is

$$V_{out} = A_v V_b = (20)(100 \text{ mV}) = 2 \text{ V rms}$$

**Related Exercise** What value of  $R_C$  in Figure 4-21 will it take to have a voltage gain of 50?

SECTION 4-4  
REVIEW

1. What is amplification?
2. How is voltage gain defined?
3. Name two factors that determine the voltage gain of an amplifier.
4. What is the voltage gain of a transistor amplifier that has an output of 5 V rms and an input of 250 mV rms?
5. A transistor connected as in Figure 4-21 has an  $r'_e = 20 \Omega$ . If  $R_C$  is 1200  $\Omega$ , what is the voltage gain?

## 4-5 ■ THE TRANSISTOR AS A SWITCH

In the previous section, we discussed the transistor as a linear amplifier. The second major application area is switching applications. When used as an electronic switch, a transistor is normally operated alternately in cutoff and saturation.

After completing this section, you should be able to

- Discuss how a transistor is used as an electronic switch
  - Define *cutoff* and *saturation*
  - Describe the conditions that produce cutoff
  - Describe the conditions that produce saturation
  - Analyze a transistor switching circuit for cutoff and saturation
  - Discuss a basic application of a transistor switching circuit

Figure 4-22 illustrates the basic operation of the transistor as a switching device. In part (a), the transistor is in the cutoff region because the base-emitter junction is not forward-biased. In this condition, there is, ideally, an *open* between collector and emitter as indicated by the switch equivalent. In part (b), the transistor is in the saturation region because the base-emitter junction and the base-collector junction are forward-biased and the base current is made large enough to cause the collector current to reach its saturation value. In this condition, there is, ideally, a *short* between collector and emitter as indi-

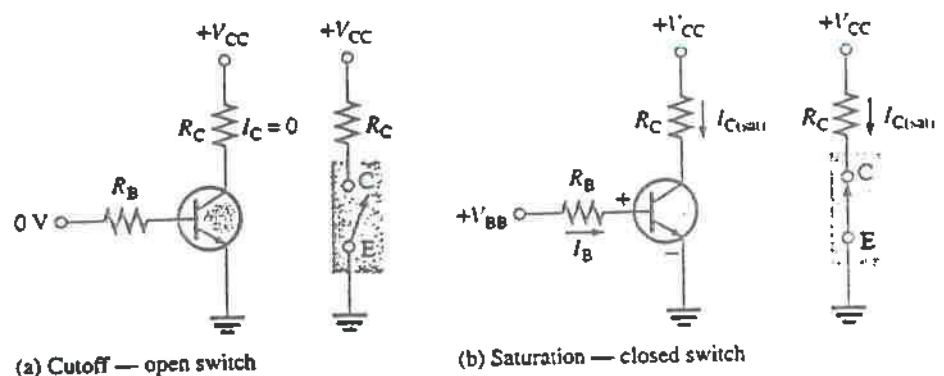


FIGURE 4-22  
Ideal switching action of a transistor.

cated by the switch equivalent. Actually, a voltage drop of up to a few tenths of a volt normally occurs, which is the saturation voltage,  $V_{CE(sat)}$ .

### Conditions in Cutoff

As mentioned before, a transistor is in the cutoff region when the base-emitter junction is *not* forward-biased. Neglecting leakage current, all of the currents are zero, and  $V_{CE}$  is equal to  $V_{CC}$ .

$$V_{CE(cutoff)} = V_{CC} \quad (4-12)$$

### Conditions in Saturation

As you have learned, when the base-emitter junction is forward-biased and there is enough base current to produce a maximum collector current, the transistor is saturated. The formula for collector saturation current is

$$I_{C(sat)} = \frac{V_{CC} - V_{CE(sat)}}{R_C} \quad (4-13)$$

Since  $V_{CE(sat)}$  is very small compared to  $V_{CC}$ , it can usually be neglected. The minimum value of base current needed to produce saturation is

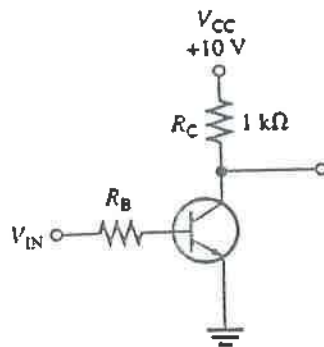
$$I_{B(min)} = \frac{I_{C(sat)}}{\beta_{DC}} \quad (4-14)$$

$I_B$  should be significantly greater than  $I_{B(min)}$  to keep the transistor well into saturation.

### EXAMPLE 4-9

- For the transistor circuit in Figure 4-23, what is  $V_{CE}$  when  $V_{IN} = 0$  V?
- What minimum value of  $I_B$  is required to saturate this transistor if  $\beta_{DC}$  is 200? Neglect  $V_{CE(sat)}$ .
- Calculate the maximum value of  $R_B$  when  $V_{IN} = 5$  V.

FIGURE 4-23



**Solution**

(a) When  $V_{IN} = 0$  V, the transistor is in cutoff (acts like an open switch) and  $V_{CE} = V_{CC} = 10$  V.

(b) Since  $V_{CE(sat)}$  is neglected (0 V),

$$I_{C(sat)} = \frac{V_{CC}}{R_C} = \frac{10 \text{ V}}{1 \text{ k}\Omega} = 10 \text{ mA}$$

$$I_B = \frac{I_{C(sat)}}{\beta_{DC}} = \frac{10 \text{ mA}}{200} = 50 \mu\text{A}$$

This is the value of  $I_B$  necessary to drive the transistor to the point of saturation. Any further increase in  $I_B$  will drive the transistor deeper into saturation but will not increase  $I_C$ .

(c) When the transistor is on,  $V_{BE} = 0.7$  V. The voltage across  $R_B$  is

$$V_{R_B} = V_{IN} - V_{BE} = 5 \text{ V} - 0.7 \text{ V} = 4.3 \text{ V}$$

Calculate the maximum value of  $R_B$  needed to allow a minimum  $I_B$  of  $50 \mu\text{A}$  by Ohm's law as follows:

$$R_B = \frac{V_{R_B}}{I_B} = \frac{4.3 \text{ V}}{50 \mu\text{A}} = 86 \text{ k}\Omega$$

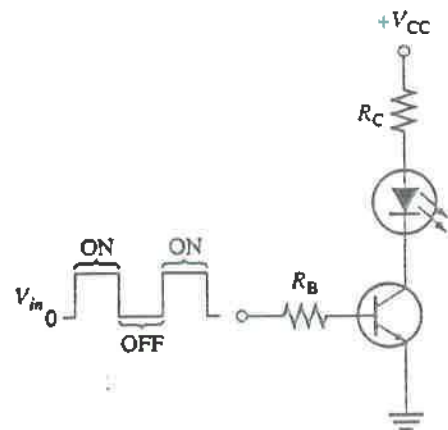
**Related Exercise** Determine the minimum value of  $I_B$  required to saturate the transistor in Figure 4-23 if  $\beta_{DC}$  is 125 and  $V_{CE(sat)}$  is 0.2 V.

**A Simple Application of a Transistor Switch**

The transistor in Figure 4-24 is used as a switch to turn the LED on and off. For example, a square wave input voltage with a period of 2 s is applied to the input as indicated. When the square wave is at 0 V, the transistor is in cutoff and, since there is no collector current, the LED does not emit light. When the square wave goes to its high level, the transistor saturates. This forward-biases the LED, and the resulting collector current through the LED causes it to emit light. So, we have a blinking LED that is on for 1 s and off for 1 s.

FIGURE 4-24

A transistor used to switch an LED on and off.



**EXAMPLE 4-10**

The LED in Figure 4-24 requires 30 mA to emit a sufficient level of light. Therefore, the collector current should be approximately 30 mA. For the following circuit values, determine the amplitude of the square wave input voltage necessary to make sure that the transistor saturates. Use double the minimum value of base current as a safety margin to ensure saturation.  $V_{CC} = 9\text{ V}$ ,  $V_{CE(\text{sat})} = 0.3\text{ V}$ ,  $R_C = 270\ \Omega$ ,  $R_B = 3.3\text{ k}\Omega$ , and  $\beta_{DC} = 50$ .

**Solution**

$$I_{C(\text{sat})} = \frac{V_{CC} - V_{CE(\text{sat})}}{R_C} = \frac{9\text{ V} - 0.3\text{ V}}{270\ \Omega} = 32.2\text{ mA}$$

$$I_{B(\text{min})} = \frac{I_{C(\text{sat})}}{\beta_{DC}} = \frac{32.2\text{ mA}}{50} = 644\ \mu\text{A}$$

To ensure saturation, use twice the value of  $I_{B(\text{min})}$ , which gives 1.29 mA. Then

$$I_B = \frac{V_{R_B}}{R_B} = \frac{V_{in} - V_{BE}}{R_B} = \frac{V_{in} - 0.7\text{ V}}{3.3\text{ k}\Omega}$$

Solve for the voltage amplitude of the square wave input  $V_{in}$ :

$$V_{in} - 0.7\text{ V} = 2I_{B(\text{min})}R_B = (1.29\text{ mA})(3.3\text{ k}\Omega)$$

$$V_{in} = (1.29\text{ mA})(3.3\text{ k}\Omega) + 0.7\text{ V} = 4.96\text{ V}$$

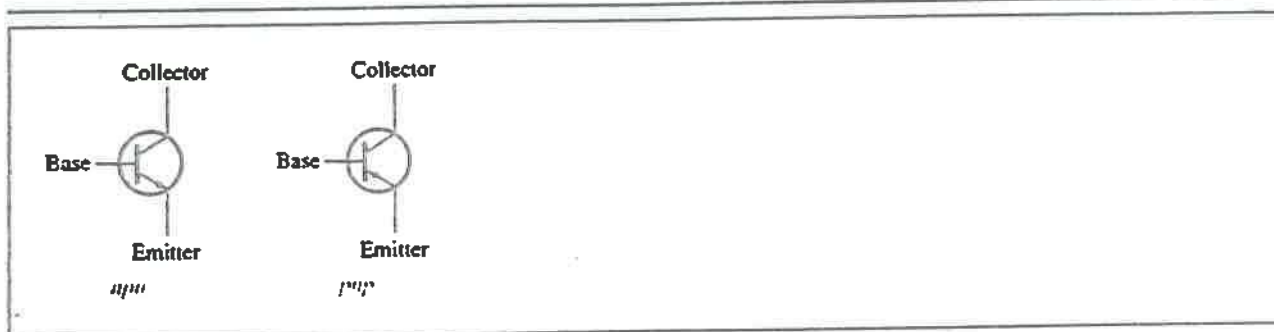
**Related Exercise** If you change the LED in Figure 4-24 to one that requires 50 mA for a specified light emission and you can't increase the input amplitude above 5 V or  $V_{CC}$  above 9 V, how would you modify the circuit? Specify the component(s) to be changed and the value(s).

**SECTION 4-5  
REVIEW**

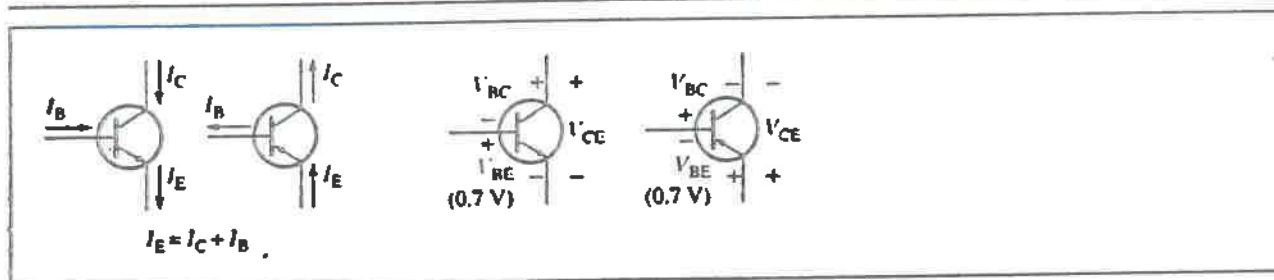
1. When a transistor is used as a switch, in what two states is it operated?
2. When is the collector current maximum?
3. When is the collector current approximately zero?
4. Under what condition is  $V_{CE} = V_{CC}$ ?
5. When is  $V_{CE}$  minimum?

## SUMMARY OF BIPOLAR JUNCTION TRANSISTORS

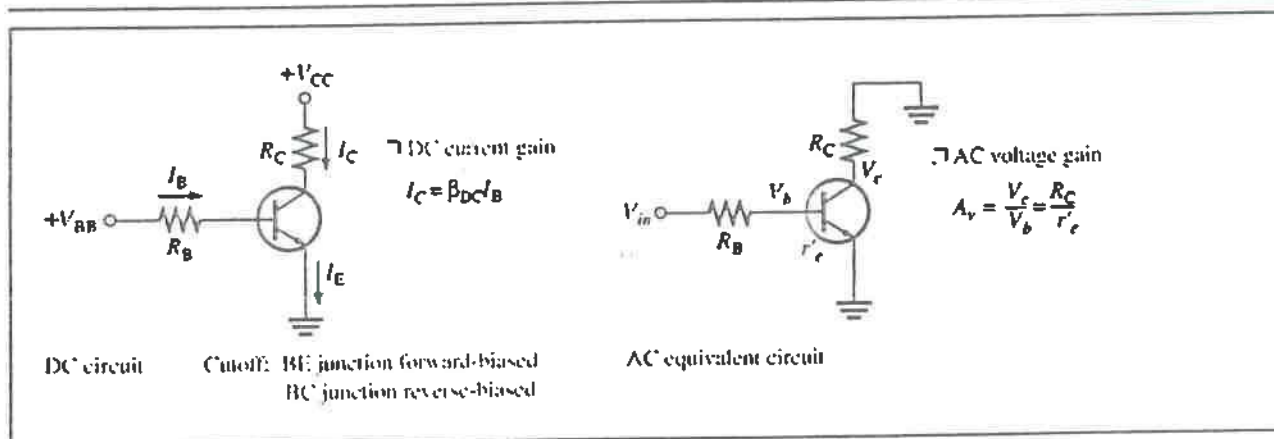
### SYMBOLS



### CURRENTS AND VOLTAGES

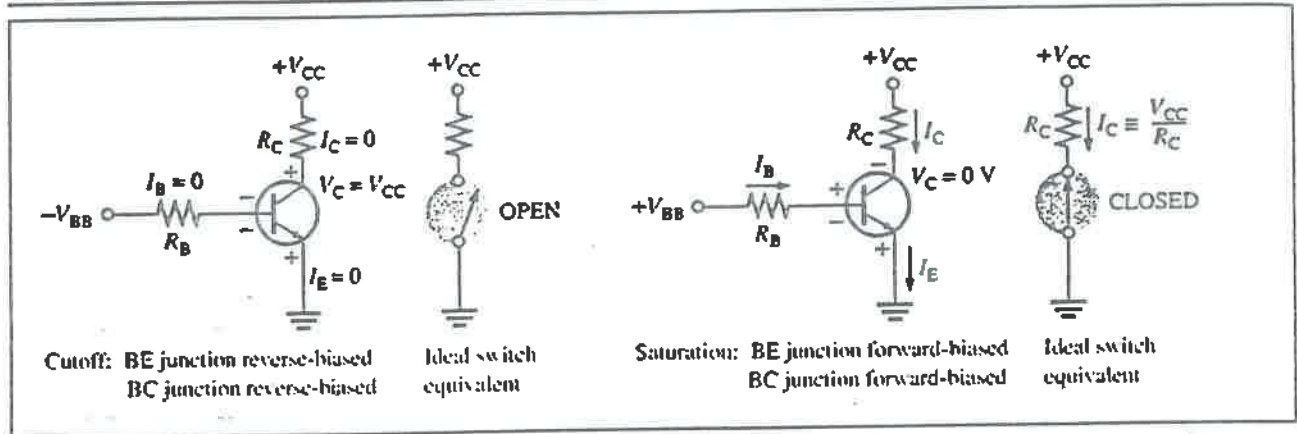


### AMPLIFICATION



SUMMARY OF BIPOLAR JUNCTION TRANSISTORS, *continued*

## CUTOFF AND SATURATION



## 4-6 ■ TRANSISTOR PACKAGES AND TERMINAL IDENTIFICATION

Transistors are available in a wide range of package types for various applications. Those with mounting studs or heat sinks are usually power transistors. Low and medium power transistors are usually found in smaller metal or plastic cases. Still another package classification is for high-frequency devices. You should be familiar with common transistor packages and be able to identify the emitter, base, and collector terminals. This section is about transistor packages and terminal identification.

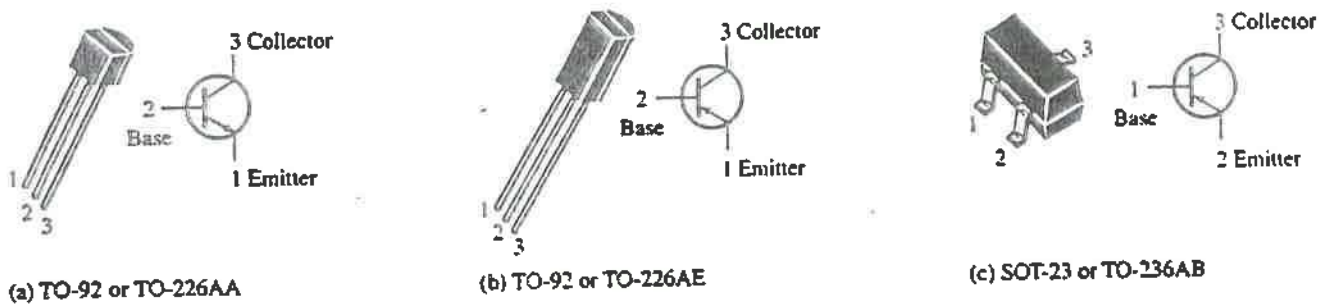
After completing this section, you should be able to

- Identify various types of transistor package configurations
  - List three broad categories of transistors
  - Recognize various types of cases and identify the pin configurations

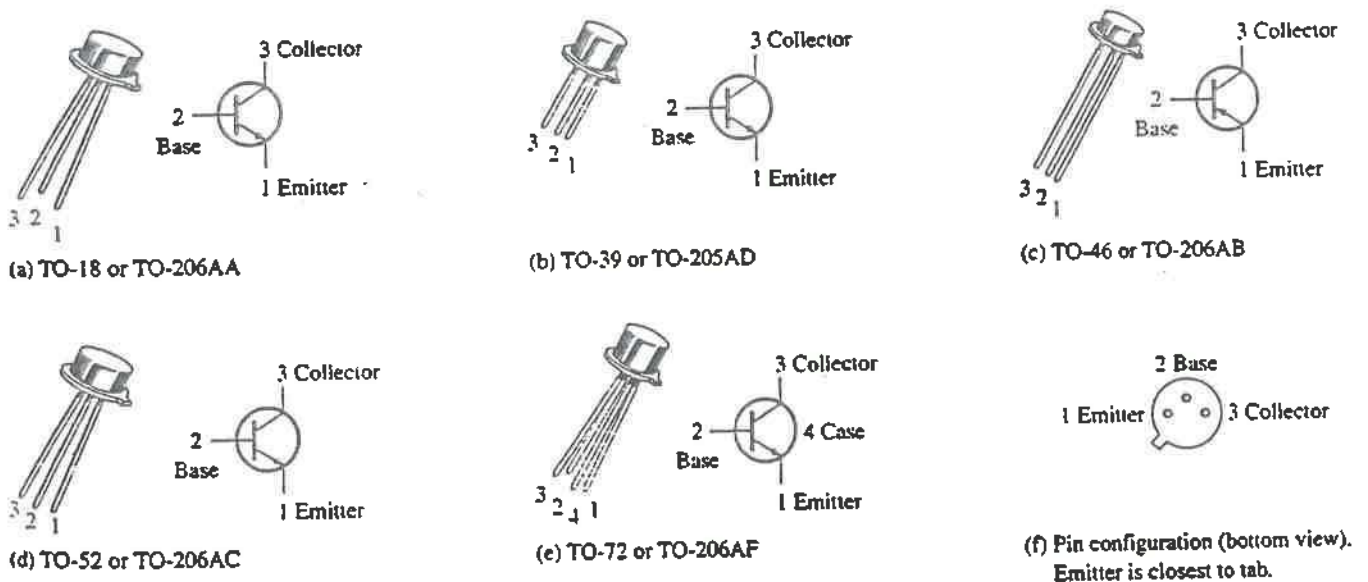
## Transistor Categories

Manufacturers generally classify their bipolar junction transistors into three broad categories: general-purpose/small-signal devices, power devices, and RF (radio frequency/microwave) devices. Although each of these categories, to a large degree, has its own unique package types, you will find certain types of packages used in more than one device category. While keeping in mind there is some overlap, we will look at transistor packages for each of the three categories, so that you will be able to recognize a transistor when you see one on a circuit board and have a good idea of what general category it is in.

**General-Purpose/Small-Signal Transistors** General-purpose/small-signal transistors are generally used for low or medium power amplifiers or switching circuits. The packages are either plastic or metal cases. Certain types of packages contain multiple transistors. Figure 4-25 illustrates common plastic cases, Figure 4-26 shows packages called *metal cans*, and Figure 4-27 shows multiple-transistor packages. Some of the multiple-transistor packages such as the dual-in-line (DIP) and the small-outline (SO) are the same as those used for many integrated circuits. Typical pin connections are shown so you can identify the emitter, base, and collector.



**FIGURE 4-25**  
 Plastic cases for general-purpose/small-signal transistors. Both old and new JEDEC TO numbers are given. Pin configurations may vary. Always check the data sheet. (Copyright of Motorola, Inc. Used by permission.)



**FIGURE 4-26**  
 Metal cases for general-purpose/small-signal transistors (copyright of Motorola, Inc. Used by permission).

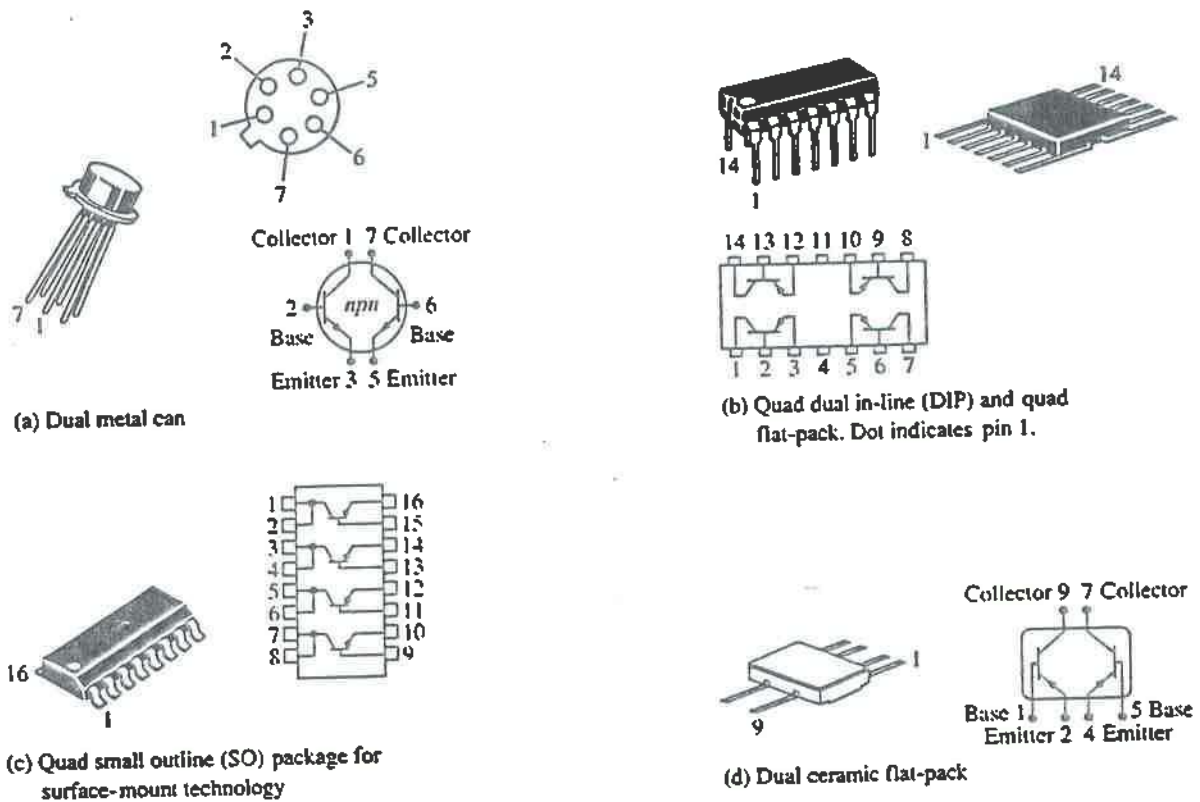


FIGURE 4-27

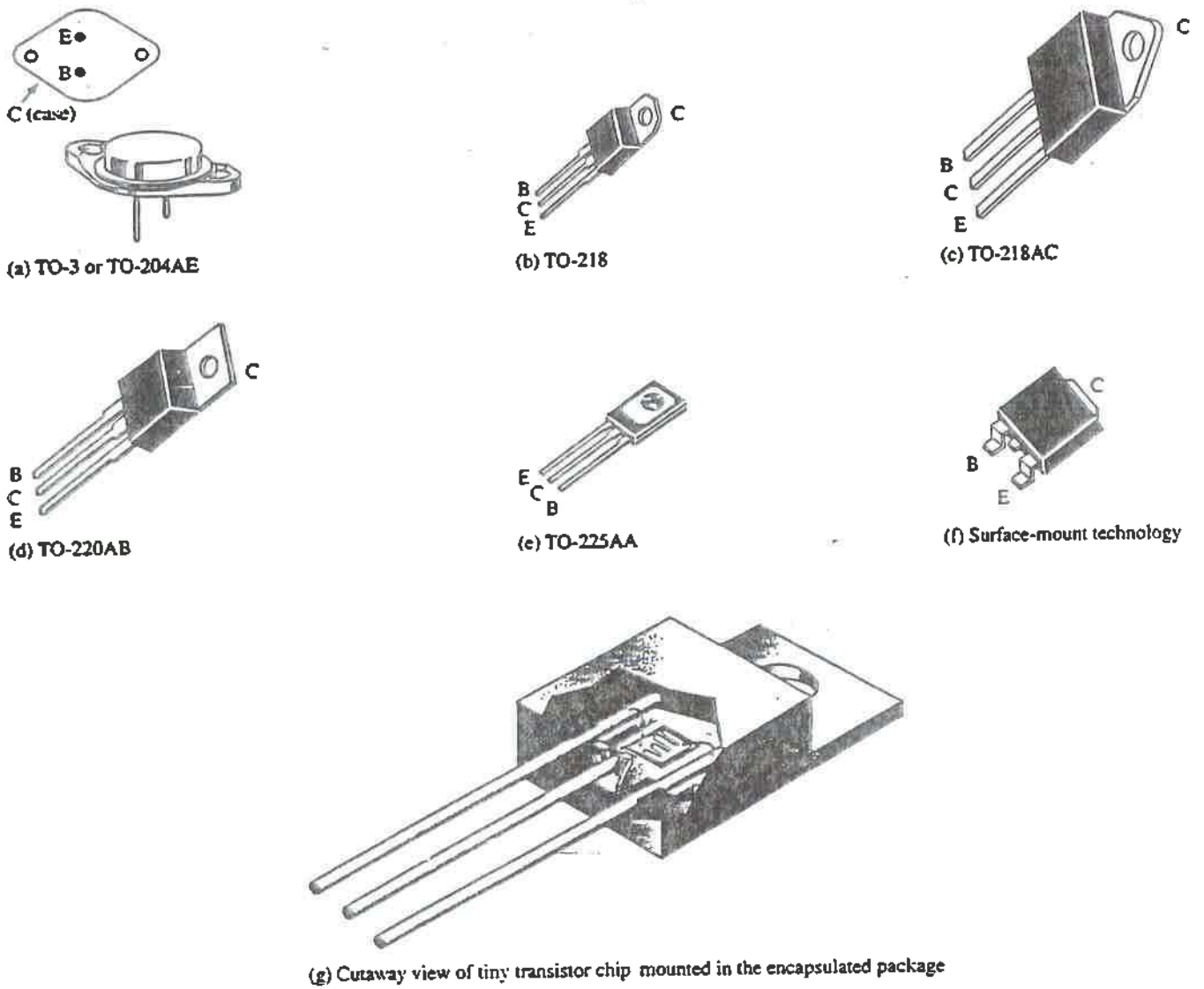
Typical multiple-transistor packages (copyright of Motorola, Inc. Used by permission).

**Power Transistors** Power transistors are used to handle large currents (typically more than 1 A) and/or large voltages. For example, the final audio stage in a stereo system uses a power transistor amplifier to drive the speakers. Figure 4-28 shows some common package configurations. In most applications, the metal tab or the metal case is common to the collector and is thermally connected to a heat sink for heat dissipation. Notice in part (g) how the small transistor chip is mounted inside the much larger package.

**RF Transistors** RF transistors are designed to operate at extremely high frequencies and are commonly used for various purposes in communications systems and other high-frequency applications. Their unusual shapes and lead configurations are designed to optimize certain high-frequency parameters. Figure 4-29 shows some examples.

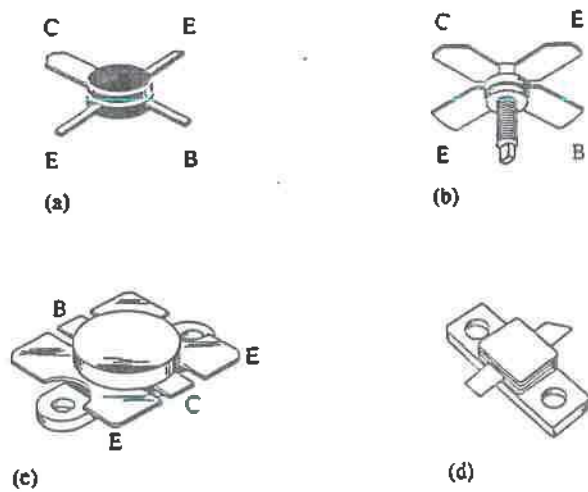
## SECTION 4-6 REVIEW

1. List the three broad categories of bipolar junction transistors.
2. In a single-transistor metal case, how do you identify the leads?
3. In power transistors, the metal mounting tab or case is connected to which transistor region?



**FIGURE 4-28**  
*Typical power transistors (copyright of Motorola, Inc. Used by permission).*

**FIGURE 4-29**  
*Examples of RF transistors (copyright of Motorola, Inc. Used by permission).*



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