

Outline

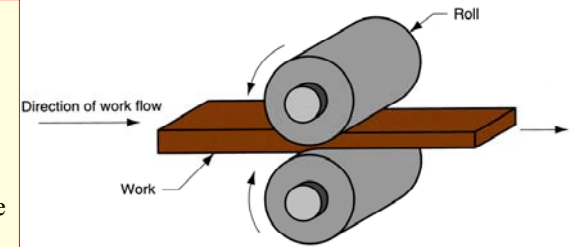
- Flat Rolling
- Other Deformation Processes Related to Rolling
 - Shape rolling, thread rolling, ring rolling
- Rolling Mills Configurations
- Rolling Analysis – Friction is *insignificant*
- Design Exercise
- Force Approximation - Friction is *significant*

Rolling

Deformation process in which work piece (slab or plate) thickness is reduced by compressive forces exerted by two opposing rolls

The rotating rolls perform two main functions:

- Pull the work into the gap between them by friction between workpart and rolls
- Simultaneously squeeze the work to reduce cross section



The rolling process (specifically, flat rolling)

Types of Rolling

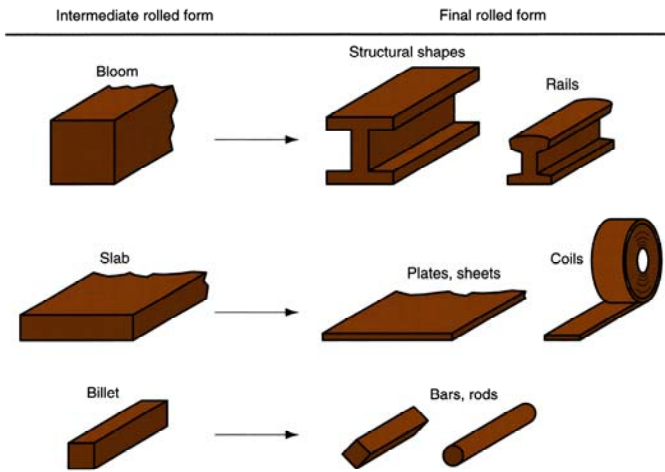
- By of work:
 - *Flat rolling* - used to reduce thickness of a rectangular cross-section
 - *Shape rolling* - a square cross-section is formed into a shape such as an I-beam
- By of work:
 - *Hot Rolling* – most common due to the large amount of deformation required
 - *Cold rolling* – produces finished sheet and plate stock

Rolling Mills



A rolling mill for hot flat rolling; (photo courtesy of Bethlehem Steel Company)

Equipment is massive and expensive



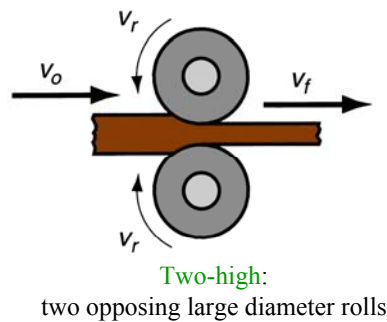
Some of the steel products made in a rolling mill

Shape Rolling

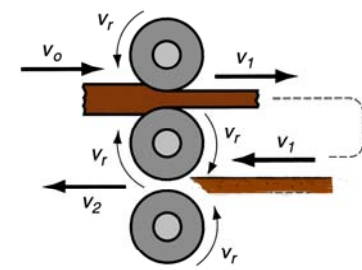
Work is deformed into a **contoured** cross-section rather than flat (rectangular)

- Accomplished by passing work through rolls that have the **reverse of desired** shape
- Products include:
 - Construction shapes such as I-beams, L-beams, and U-channels
 - Rails for railroad tracks
 - Round and square bars and rods

Rolling Mills Configurations

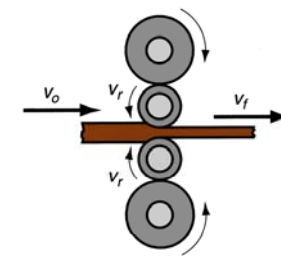


Two-high:
two opposing large diameter rolls

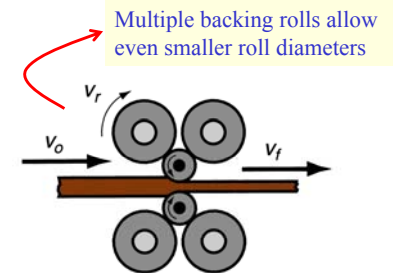


Three-high:
work passes through both directions

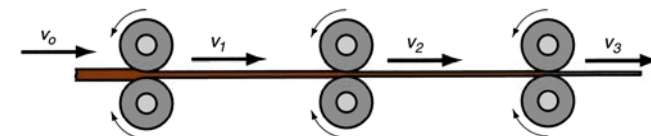
Rolling Mills Configurations



Four-high:
backing rolls support smaller work rolls



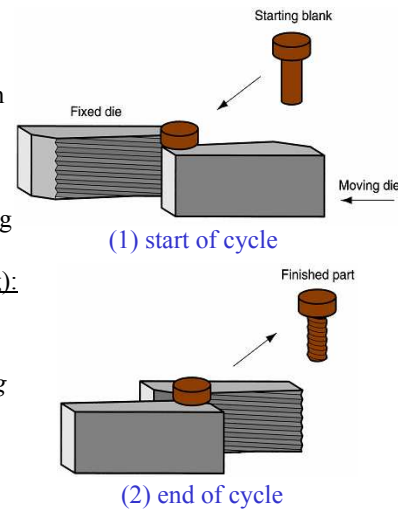
Cluster mill:
multiple backing rolls on smaller rolls



Tandem rolling mill: sequence of two-high mills

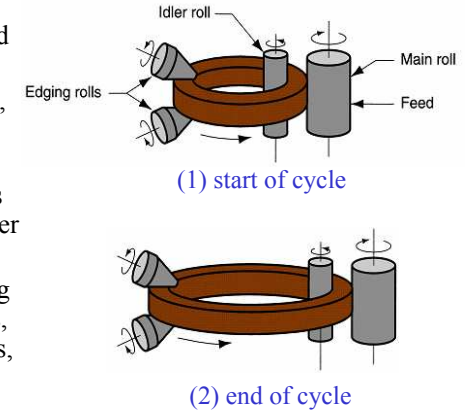
Thread Rolling

- Bulk deformation process used to form **threads on cylindrical** parts by rolling them between two dies
- Most important **commercial** process for **mass producing** bolts and screws
- Performed by **cold working** in thread rolling machines
- Advantages over thread cutting (machining):
 - Higher production rates
 - Better material **utilization**
 - Stronger threads due to **work hardening**
 - Better **fatigue** resistance due to compressive stresses introduced by rolling



Ring Rolling

- Deformation process in which a **thick-walled ring of smaller diameter** is rolled into a **thin-walled ring of larger diameter**
- As thick-walled ring is compressed, deformed metal elongates, causing diameter of ring to be enlarged
- **Hot working** process for large rings and **cold working** process for smaller rings
- Applications: ball and roller bearing races, steel tires for railroad wheels, and rings for pipes, pressure vessels, and rotating machinery
- Advantages: material **savings**, ideal **grain orientation**, **strengthening** through cold working



Flat Rolling – Terminology

Draft = amount of thickness reduction:

$$d = t_o - t_f$$

Where:

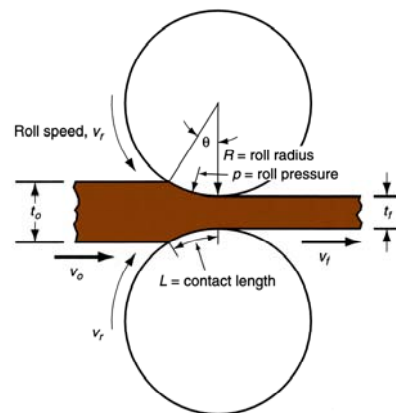
d = draft

t_o = starting thickness

t_f = final thickness

Reduction = draft expressed as a fraction of starting stock thickness:

$$r = \frac{d}{t_o}$$



Side view of flat rolling, indicating before and after thicknesses, work velocities, angle of contact with rolls, and other features

Flat Rolling – Terminology

- **Friction** at the entrance controls the maximum possible draft.

$$d_{\max} = \mu^2 R$$

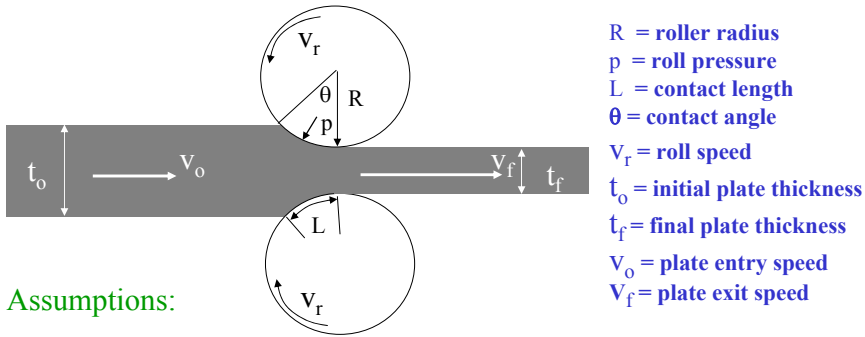
d_{\max} = Maximum draft (mm)
 μ = coefficient of friction
 R = Roll Radius (mm)

- However, it depends on lubrication, work-piece and roller materials and temperature.

$$\mu = \begin{cases} 0.1 & \text{for coldworking} \\ 0.2 & \text{for warmworking} \\ 0.3 & \text{for hotworking} \end{cases}$$

- When sticking occurs, μ can be as high as **0.7**

Rolling Analysis



R = roller radius
 p = roll pressure
 L = contact length
 θ = contact angle
 v_r = roll speed
 t_0 = initial plate thickness
 t_f = final plate thickness
 v_0 = plate entry speed
 v_f = plate exit speed

Assumptions:

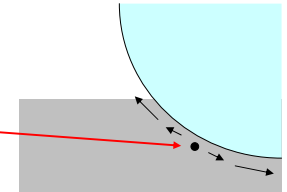
- Infinite sheet
- Uniform, perfectly rigid rollers
- Constant material volume:
 $t_0 w_0 L_0 = t_f w_f L_f$
 $\Rightarrow t_0 w_0 v_0 = t_f w_f v_f$ (flow rate)

where

L_0 = initial plate length
 L_f = final plate length

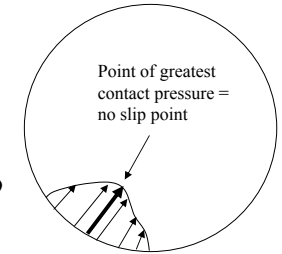
Rolling Analysis

- Slipping and friction on the contact arc except on no-slip point (neutral point)
 - One point along the arc where work velocity equals roll velocity.
- Amount of slip between the work and the rolls: **Forward slip**



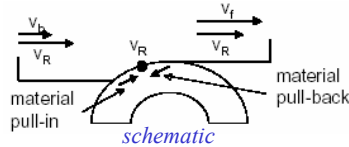
$$s = \frac{v_f - v_r}{v_r}$$

Does it make sense that $v_r < v_f$?

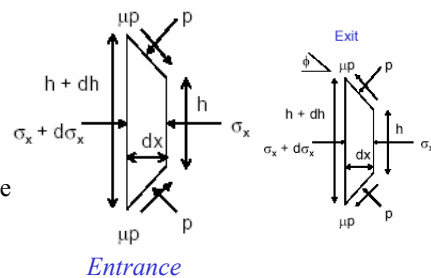


Rolling Analysis

- **Entrance:** material is pulled into the nip
 - roller is moving **faster** than material
- **Exit:** material is pulled back into nip
 - roller is moving **slower** than material



- Frictional forces between roller and material must be in **balance**.
 - otherwise material will be torn apart
- Hence, the zero point must be where the **two pressure equations are**



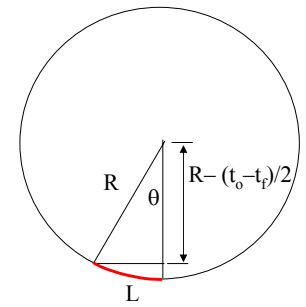
Rolling Analysis

- Define true strain $\epsilon = \ln \frac{t_0}{t_f}$ (Note: use t_0/t_f to keep > 0)
- Apply average flow stress $\bar{Y}_f = \frac{K \epsilon^n}{1+n}$
- Approximate roll force:
 - If friction is not significant, i.e. $\frac{h_{avg}}{L} \gg 1$

$$F = w \int_0^L p dL = \bar{Y}_f w L$$

$$\text{where } L = \sqrt{R(t_0 - t_f)}$$

- Torque estimated by $T/\text{roller} = 0.5 F L$
- Power = $P = T\omega = 2\pi N F L$ (for two rollers)



Example

Roll a 12 inch wide strip which is 1 inch thick, to 0.875 inch thickness in one pass with roll speed of 50 rpm and radius = 10 inches. Material has $K = 40,000$ psi, $n = 0.15$ and $\mu = 0.12$.

Is this a feasible process? If so calculate F , T , and power. (*Assume friction is not significant!*)

Force Approximation: Large Rolls

Large Reduction and Significant Friction

$$\frac{h_{ave}}{L} \ll 1 \quad \text{Friction is significant}$$

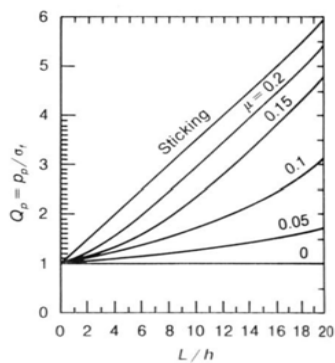
$$P_{ave} = \bar{Y}_f \left(1 + \frac{\mu L}{2h_{ave}} \right)$$

$$F/roller = Lw\bar{Y}_f \left(1 + \frac{\mu L}{2h_{ave}} \right)$$

$$\bar{Y}' = 1.15\bar{Y} = 1.15 \times \frac{K\varepsilon^n}{n+1}$$

- The last equation can be used in both cases, *i.e.* when friction is significant or not.
- It is an approximation using the distortion-energy criterion for plane strain (**von Mises**). [see 6.2.2 Kalpakjian]

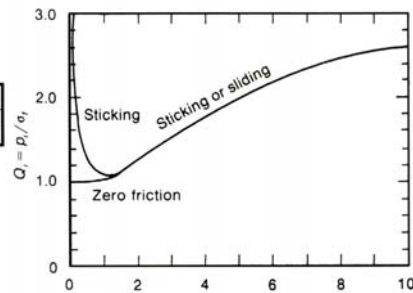
Interface Pressure: h/L ratio



When $h/L > 1.0 \Rightarrow$ Inhomogeneous deformation and use Q_i

When $h/L < 1.0 \Rightarrow$ Frictional effects are more severe use Q_p

$$Q_i = \frac{P_i}{\sigma_f}$$



Average pressures in upsetting a rectangular slab increase with friction and L/h ratio. (After J. F. W. Bishop, *Quart. J. Mech. Appl. Math.* 9:236-246 (1956). With permission of Pergamon Press.)

$$F = (1.15)\bar{Y}_f Q_i L W$$

$$F = (1.15)\bar{Y}_f Q_p L W$$

$h/L \rightarrow$
Pressure needed to indent a workpiece

Next time
Extrusion